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## Course Overview

ARDOT Specifications



Materials / Terminology  
Volumetrics / Calculations  
Sampling / Reduction  
Gyratory Compaction  
Gmb / Gmm  
Binder Content  
Compaction  
Quality Control / Quality Assurance

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# Test Day

## Written Exam

- ≈ 60 Questions
- Closed Book Exam
  - 2 Hour Time Limit
  - 70 % Overall Required to Pass

## Results

- [www.cttp.org](http://www.cttp.org)
- Letter & Certification
- 5 Year Certification
- Basic Aggregates

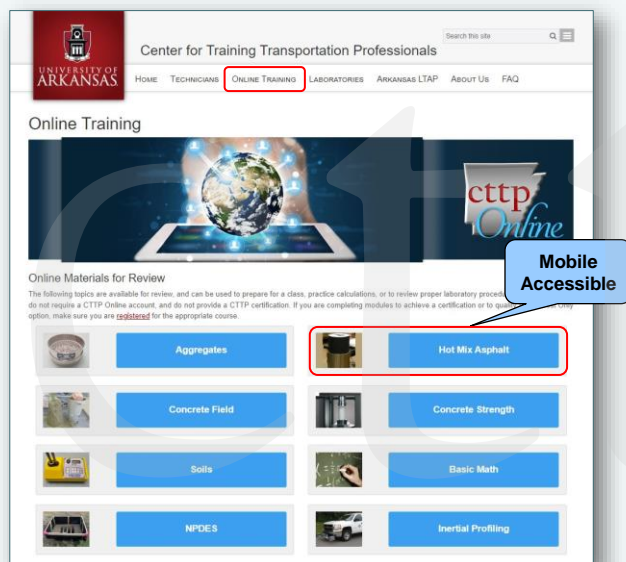
## Performance Exam

- 5 Exam Stations
  - Bulk SpG (Gmb)
  - Max SpG (Gmm)
  - Gyratory Compaction
  - Ignition Oven
  - AC Gauge
- 2 attempts



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## Help?

If you need help with mathematical calculations, just ask. Your instructor will be happy to assist you.

If you need further practice or assistance, please see our website [www.cttp.org](http://www.cttp.org) for online training.

- Modules
- Videos
- Practice Problems

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## Materials



Aggregate (stone) – granular material

Binder – an asphalt-based cement (Performance Graded)

Asphalt Mixture – Binder and aggregate combined

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## Mix Design vs Production

### Mix Design

Combinations of aggregates and binder to determine optimum properties

- Volumetric
- Material quality
- Performance

### Production

Ensure that the mix matches the design by performing regular checks of mix properties

- Specifications
- Tolerances
- Pay items

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# Aggregates

## Nominal Maximum Aggregate Size (NMAS)

- Superpave – one size larger than the 1<sup>st</sup> sieve to retain >10%

## Maximum Aggregate Size (MAS)

- Superpave – One size larger than NMAS

## ARDOT mix designs based on NMAS

- Surface: 12.5mm (1/2"), 9.5mm (3/8")
- Binder: 25.0mm (1")
- Base: 37.5mm (1-1/2")



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# Aggregate Properties

Gradation

Angularity

Fractured faces

Flat/Elongated

Durability

Soundness



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## Aggregate Blend Gradation



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## Binder Properties

Temperature – Viscosity

Climate & Traffic

Performance Graded

- PG 64-22
- PG 70-22
- PG 76-22

Mixing Temperature

Compaction Temperature



**PG**



**64°C**



**-22°C**

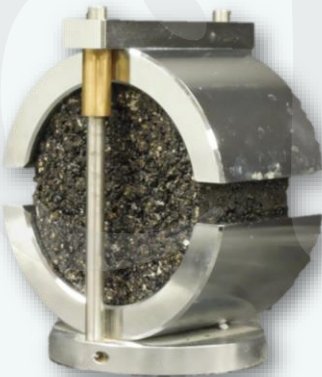
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## Performance Properties

### Water Sensitivity

- Antistrip



### Wheel Tracking Test

- Rutting Susceptibility

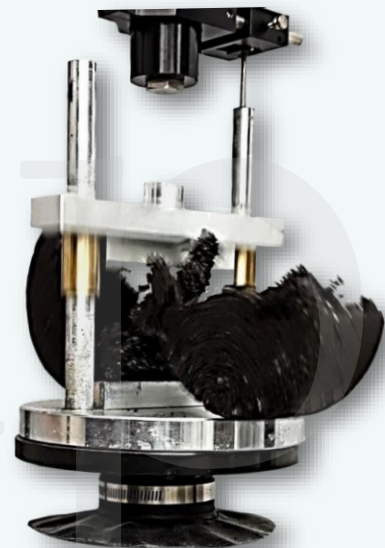


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## Balanced Mix Design

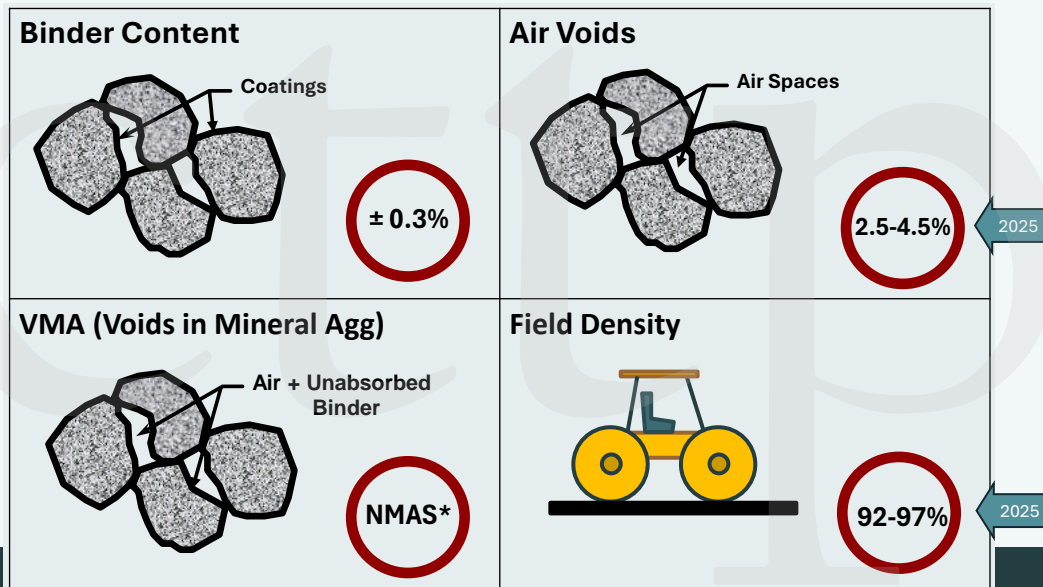
Rutting  
Cracking



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## Mix Properties / Pay Items



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## Terminology

 $X_{yz}$ 
**X**

Quantity

G: specific gravity  
 W: weight (mass)  
 V: volume  
 P: percent

**y**

Material

a: air  
 b: binder  
 s: stone (aggregate)  
 m: mix

**z**

Type

a: absorbed  
 b: bulk  
 e: effective  
 m: maximum

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## Terminology

Term	Definition
Pb	
Gsb	
Pba	
Gmm	
Gse	

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## Percent Binder & Percent Stone



$$\begin{array}{ccccc}
 \text{Agg Wt} & + & \text{Binder Wt} & = & \text{Mix Wt} \\
 P_s & + & P_b & = & 100 \%
 \end{array}$$

$$P_s = \frac{\text{Agg Wt}}{\text{Mix Wt}} \times 100 \qquad P_b = \frac{\text{Binder Wt}}{\text{Mix Wt}} \times 100 \qquad \text{Mix Wt} = \frac{\text{Agg Wt}}{P_s} \times 100$$

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## % Binder and % Stone

Determine the  $P_s$  if the  $P_b = 5.8 \%$

$$P_s + P_b = 100 \%$$

$$P_s = 100 - 5.8 = 94.2$$

**94.2 %**

*Report  $P_s$  &  $P_b$  to the nearest 0.1 %*

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## % Binder and % Stone

Determine the  $P_s$  if the  $P_b = 6.1 \%$

$$P_s + P_b = 100 \%$$

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## Specific Gravity of Binder ( $G_b$ )

### Mix Design

- 77 °F

What is the  $G_{b_{77}}$  for binder with a  $G_{b_{60}} = 1.024$ ?

### Field Testing

- Convert  $G_b$  from 60 °F to 77 °F
- Calculations use  $G_{b_{77}}$

$$G_{b_{77}} = (1.024)(0.9941) = 1.01795...$$

### Conversion

$$G_{b_{77}} = (G_{b_{60}})(0.9941)$$

**1.018**

*Report all specific gravities to the nearest 0.001*

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## Specific Gravity of Binder ( $G_b$ )

Determine the specific gravity needed for calculations

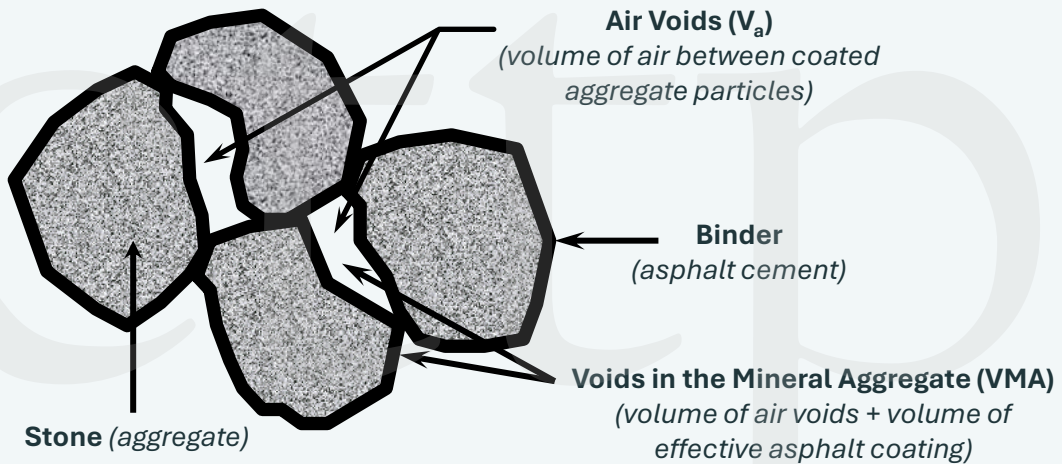
$$G_{b_{60}} = 1.028$$

$$G_{b_{77}} = (G_{b_{60}})(0.9941)$$

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## Terminology



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## Mass – Volume Relationships

### Aggregate

- Mass (wt)
- Volume

### Binder

- Mass (wt)
- Volume

### Air

- Volume

$$\text{Density} = \frac{\text{Weight}}{\text{Volume}}$$

Weight		Volume
n/a	<b>Air</b>	$V_a$
$W_b$	<b>Binder</b>	$V_b$
$W_s$	<b>Aggregate</b>	$V_s$

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## Bulk Specific Gravity of the Mix ( $G_{mb}$ )

Describes the density of the mix when compacted

- Will have some air voids



Weight		Volume
n/a	Air	$V_a$
$W_b$	Binder	$V_b$
$W_s$	Aggregate	$V_s$

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## Calculation of $G_{mb}$

$$G_{mb} = \frac{A}{(B - C)}$$

A = Dry mass of specimen

B = SSD mass of specimen

C = Submerged mass of specimen

*Report  $G_{mb}$  to 0.001*

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## Calculation of G<sub>mb</sub>

Determine the G<sub>mb</sub> of the compacted specimen

Dry Mass	4456.7	<b>A</b>
Submerged Mass	2521.0	<b>C</b>
SSD Mass	4463.5	<b>B</b>

$$G_{mb} = \frac{A}{(B - C)}$$

$$G_{mb} = \frac{4456.7}{(4463.5 - 2521.0)} = \frac{4456.7}{1942.5} = 2.29431...$$

**2.294**

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## Calculation of G<sub>mb</sub>

Determine the G<sub>mb</sub> of the compacted specimen

Dry Mass	4498.0	<b>A</b>
Submerged Mass	2496.3	<b>C</b>
SSD Mass	4502.0	<b>B</b>

$$G_{mb} = \frac{A}{(B - C)}$$

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## Calculation of Absorption

$$\% \text{ Abs} = \frac{(B - A)}{(B - C)} \times 100 \%$$

A = Dry mass of specimen  
B = SSD mass of specimen  
C = Submerged mass of specimen

*Report % Abs to 0.01 %*

Weight		Volume
n/a	Air	$V_a$
$W_b$	Binder	$V_b$
$W_s$	Aggregate	$V_s$

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## % Absorption (% Abs)

Determine the % absorption of the compacted specimen

Dry Mass = 4571.6 g **A**  
Subm. Mass = 2633.0 g **C**  
SSD Mass = 4585.1 g **B**

$$\% \text{ Abs} = \frac{(B - A)}{(B - C)} \times 100$$

$$\% \text{ Abs} = \frac{(4585.1 - 4571.6)}{(4585.1 - 2633.0)} \times 100 = \frac{13.5}{1952.1} \times 100 \% = 0.69156...$$

**0.69 %**

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## % Absorption (% Abs)

Determine the % absorption of the compacted specimen

Dry Mass = 3568.2 g  
 Subm. Mass = 2016.1 g  
 SSD Mass = 3577.9 g

$$\% \text{ Abs} = \frac{(B - A)}{(B - C)} \times 100$$

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## Theoretical Maximum Density of the Mix (Gmm)

Maximum Theoretical Specific Gravity of the Mixture (Gmm)

- “Rice” method
- Density of mixture with no air voids



Weight		Volume
n/a	Air	n/a
W <sub>b</sub>	Binder	V <sub>b</sub>
W <sub>s</sub>	Aggregate	V <sub>s</sub>

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## Calculating Rice (Gmm)

Specific gravity of mixture with no air voids

- Used to determine relative density and % compaction
- Serves as a baseline value for maximum density

$$G_{mm} = \frac{A}{(A - C)}$$

*A = dry mass*

*C = submerged mass*



*Report all specific gravities to the nearest 0.001*

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## Calculating Gmm

Determine the  $G_{mm}$  of the asphalt mixture

Dry Mass	1796.4	<b>A</b>
Sub Mass (Bowl + S)	2348.7	<b>C = 1048.7</b>
Sub Mass (Bowl)	1300.0	

$$G_{mm} = \frac{A}{(A - C)}$$

$$G_{mm} = \frac{1796.4}{(1796.4 - 1048.7)} = \frac{1796.4}{747.7} = 2.40256...$$

**2.403**

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## Calculating G<sub>mm</sub>

Determine the G<sub>mm</sub> of the asphalt mixture

Dry Mass	2737.6
Sub Mass (Bowl + S)	2948.2
Sub Mass (Bowl)	1300.0

$$G_{mm} = \frac{A}{(A - C)}$$

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## % Density (based on G<sub>mm</sub>)

Density of a mixture relative to a standard

- Maximum Theoretical Specific Gravity

$$\% \text{ Density} = \frac{G_{mb}}{G_{mm}} \times 100$$



*Report % density to the nearest 0.1 %*

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## % Density (based on Gmm)

Determine the % density

$G_{mb}$ of Core	2.327
$G_{mm}$ of Mix	2.434

$$\% \text{ Density} = \frac{G_{mb}}{G_{mm}} \times 100$$

$$\% \text{ Density} = \frac{2.327}{2.434} \times 100 = 95.6039\ldots$$

**95.6 %**

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## % Density (based on Gmm)

Determine the % density

$G_{mb}$ of Core	2.358
$G_{mm}$ of Mix	2.512

$$\% \text{ Density} = \frac{G_{mb}}{G_{mm}} \times 100$$

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## % Air Voids ( $V_a$ )

Volume of air pockets in a compacted asphalt mixture

$$V_a = 100 - \% \text{ Density}$$

$$V_a = 100 - \left( \frac{G_{mb}}{G_{mm}} \times 100 \right)$$

$$\text{or} \left( 1 - \frac{G_{mb}}{G_{mm}} \right) \times 100$$

Report % air voids to the nearest 0.1 %

Weight		Volume
n/a	Air	$V_a$
$W_b$	Binder	$V_b$
$W_s$	Aggregate	$V_s$

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## % Air Voids ( $V_a$ )

Find the reported % air voids

$G_{mb}$  1      2.361

$G_{mb}$  2      2.367

Average  $G_{mb}$     2.364

$G_{mm}$       2.447

$$V_a = 100 - \left( \frac{G_{mb}}{G_{mm}} \times 100 \right)$$

$$V_a = 100 - \left( \frac{2.364}{2.447} \times 100 \right) = 100 - 96.608... = 3.3919...$$

**3.4 %**

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## % Air Voids ( $V_a$ )

Find the reported % air voids

$G_{mb}$  1      2.309  
 $G_{mb}$  2      2.303

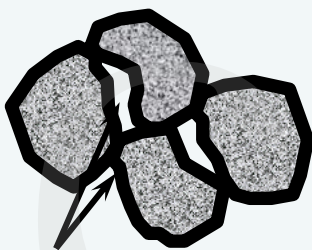
$G_{mm}$       2.415

$$V_a = 100 - \left( \frac{G_{mb}}{G_{mm}} \times 100 \right)$$

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## Voids in the Mineral Aggregate (VMA)



**Voids in the Mineral Aggregate (VMA)**  
 (volume of air voids  
 + volume of effective  
 asphalt coating)

$$VMA = 100 - \left[ \frac{(G_{mb})(P_s)}{G_{sb}} \right]$$

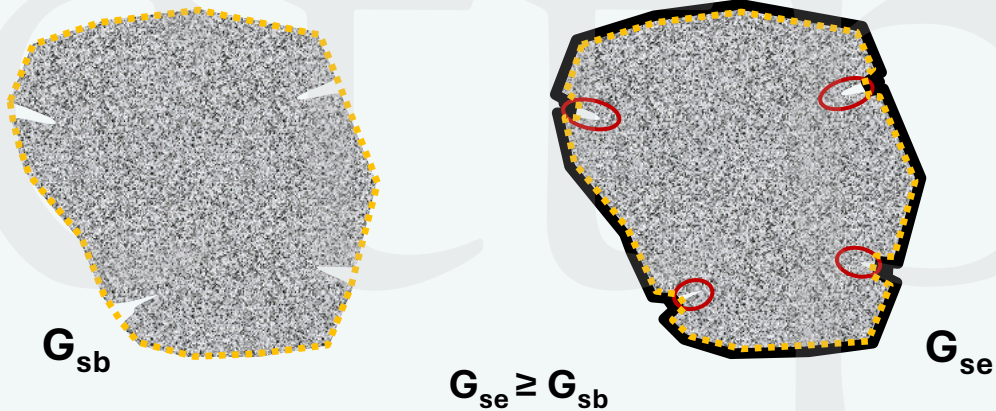
$$VMA_{eff} = 100 - \left[ \frac{(G_{mb})(P_s)}{G_{se}} \right]$$

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## Effective Specific Gravity of Aggregate ( $G_{se}$ )

Specific gravity of aggregate including the volume of pervious pore spaces not filled with asphalt



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## Calculating $G_{se}$

$$\frac{P_s}{G_{se}} + \frac{P_b}{G_b} = \frac{100}{G_{mm}}$$

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## Calculating G<sub>se</sub>

$$G_{se} = \frac{P_s}{\left( \frac{100}{G_{mm}} - \frac{P_b}{G_b} \right)}$$

*Report all specific gravities to the nearest 0.001*

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## Calculating G<sub>se</sub>

Determine the G<sub>se</sub> of the mixture

P <sub>b</sub>	5.7 %
G <sub>mm</sub>	2.413
G <sub>b77</sub>	1.032

$$G_{se} = \frac{P_s}{\left( \frac{100}{G_{mm}} - \frac{P_b}{G_b} \right)}$$

$$P_s = 100 - 5.7 = 94.3$$

$$G_{se} = \frac{94.3}{\left( \frac{100}{2.413} - \frac{5.7}{1.032} \right)} = \frac{94.3}{(41.4421... - 5.5232...)} = \frac{94.3}{35.9189...} = 2.62535...$$

**2.625**

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## Calculating G<sub>se</sub>

Determine the G<sub>se</sub> of the mixture

P <sub>b</sub>	4.2 %
G <sub>mm</sub>	2.555
G <sub>b60</sub>	1.032

$$G_{se} = \frac{P_s}{\left( \frac{100}{G_{mm}} - \frac{P_b}{G_b} \right)}$$

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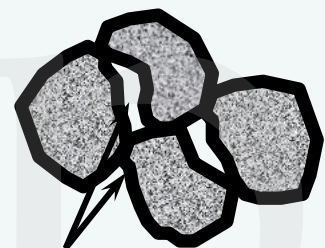
## Voids in the Mineral Aggregate (VMA)

(VMA<sub>eff</sub>) – (VMA) = VMA correction factor, or “VMA<sub>CF</sub>”

$$VMA_{eff} = 100 - \left[ \frac{(G_{mb})(P_s)}{G_{se}} \right]$$

$$VMA = VMA_{eff} - VMA_{CF}$$

*Report % VMA to the nearest 0.1 %*



**Voids in the Mineral Aggregate (VMA)**  
(volume of air voids  
+ volume of effective  
asphalt coating)

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## Voids in the Mineral Aggregate (VMA)

Calculate the % VMA for the mixture

$G_{mb}$  1 2.345

$G_{mb}$  2 2.343

Average  $G_{mb}$  2.344

$P_b$  4.1 %

$P_s$  95.9 %

$VMA_{CF}$  0.3 %

$G_{se}$  2.588

$$VMA_{eff} = 100 - \left[ \frac{(G_{mb})(P_s)}{G_{se}} \right]$$

$$VMA = VMA_{eff} - VMA_{CF}$$

$$VMA_{eff} = 100 - \left[ \frac{(2.344)(95.9)}{2.588} \right] = 100 - 86.858... = 13.1$$

$$VMA = 13.1 - 0.3 = 12.8$$

**12.8 %**

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## Voids in the Mineral Aggregate (VMA)

Calculate the % VMA for the mixture

$G_{mb}$  1 2.425

$G_{mb}$  2 2.431

$P_b$  4.4 %

$VMA_{CF}$  0.5 %

$G_{se}$  2.635

$$VMA_{eff} = 100 - \left[ \frac{(G_{mb})(P_s)}{G_{se}} \right]$$

$$VMA = VMA_{eff} - VMA_{CF}$$

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## ARDOT Mix Design

The mix design for the 25.0 mm ACHM Binder is accepted. Average verification results on this mix design are: Air Voids – 4.0 %; Gmb – 2.340; Height at Ndes – 115.2 mm. This mix design will be identified as HMA 684-25 for the Hogville, Inc. – Plant #1 in Fayetteville, AR.

### Mix Design Properties

Optimum Asphalt Binder:	4.1 %	
Air Voids:	4.0 %	
VMA:	13.0 %	
VFA:	69.2 %	
Fines to Asphalt Ratio:	0.74	
Retained Stability:	94.1 %	
Ndes:	75	
Asphalt Binder:	HOG OIL PG 70-22	
APA Results:	1.951 mm	5.000 mm or less

Mix Design Handout – p. 1

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## Volumetric Mix Design

No.	Aggr. ID	Aggr. Name	Source	
1	75942	C Rock	Hogville Group, Hog Quarry	Fayetteville, AR
2	75861	5/8" Chips	Hogville Group, Hog Quarry	Fayetteville, AR
3	38850	1/4" Screenings	Hogville Group, Hog Quarry	Fayetteville, AR
4	22200	Man. Sand	Pork City Materials	Fayetteville, AR
5	02914	Sand	Hogville Group, Hog Quarry	Fayetteville, AR

Aggregates							Job	Control
Sieve Size	1	2	3	4	5		Mix	Points
50	100	100	100	100	100		100	100%
37.5	100	100	100	100	100		100	100%
25	72	100	100	100	100		100	90-100%
19	35	100	100	100	100		100	90% Max
12.5	11	89	100	100	100		93	
9.5	7	59	100	92	100		83	
4.75	4	7	90	55	100		59	
2.36	3	3	61	30	100		34	19-45%
1.18	2	3	37	17	99		22	
0.6	2	2	21	11	92		15	
0.3	2	2	11	7	63		8	
0.15	2	2	4	5	16		6	
0.075	1.8	2.0	3.3	4.7	13.2		4.8	1-7%
Cold Feed%	28	25	29	15	3			
Gsb	2.570	2.557	2.614	2.556	2.599			

Mix Design Handout – p. 2

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# Volumetric Mix Design

## Design Summary

Mix Design #: HMA684-25

Mix Type: 25.0 MM ACHM Binder

Total Asphalt Content %:	<u>4.1</u>	Air Voids (Va):	<u>4.0</u>
New Asphalt Content %:	<u>4.1</u>	VMA:	<u>13.0</u>
Max. Theor. SG (Gmm):	<u>2.437</u>	VMA Corr. Factor:	<u>0.3</u>
Asphalt Binder:	<u>PG 70-22</u>	Gsb:	<u>2.578</u>
Asphalt Binder Source:	<u>Hog Oil Company</u>	Gse:	<u>2.588</u>
Mixing Temp (F):	<u>330</u>	Gb:	<u>1.031</u>
Compaction Temp (F):	<u>305</u>	Ni:	<u>7</u>
Antistrip Source:	<u>HogGrip 975</u>	Ndes:	<u>75</u>
Antistrip %:	<u>0.25</u>	Nmax:	<u>115</u>
% Retained Stability:	<u>94.1</u>		
APA Results:	<u>1.951</u>	Spec Max = 5.000 mm	

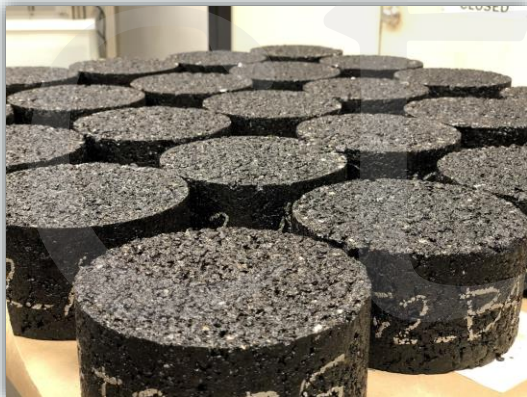
Mix Design Handout – p. 3

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## Mix Design

### Volumetric Proportions



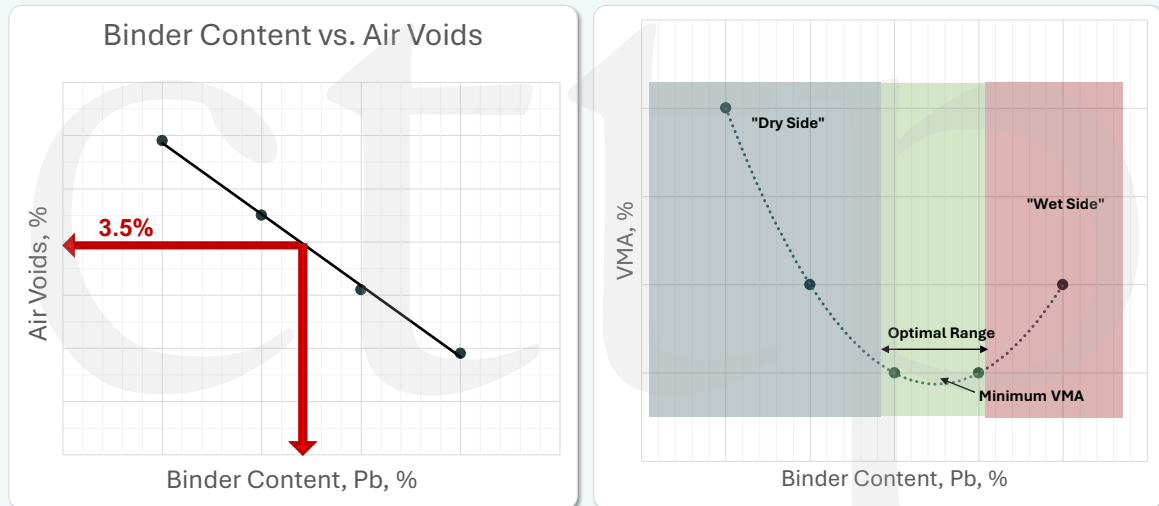
### Performance



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## Volumetric Proportions



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## Performance – Moisture Sensitivity

Effects of water on strength of compacted mix

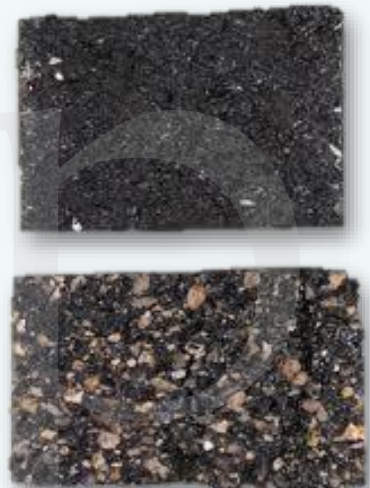
- 6" Marshall breaking head

Specimens in 2 groups

- Group A – control
- Group B – conditioned

Minimum Water Sensitivity Ratio = **80%**

SS-400-6: All ACHM mixes must contain liquid antistrip additive

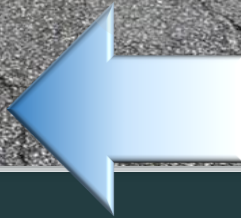


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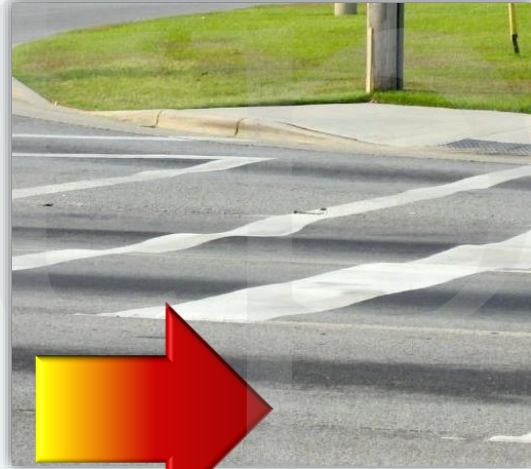
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# Pavement Distresses

Cracking



Rutting



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## Rutting – APA

### Aging

- 2 hrs at Compaction Temp

### Specimens

- 150 mm diameter
- 75 mm height
- $7 \pm 1.0$  % air voids
- 100 psi, 64 °C

### Criteria

- Max of 5 or 8 mm @ 8000 cycles



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## Cracking Test – IDEAL-CT

### Aging

- 2 hrs at Compaction Temp

### Specimens

- 3 specimens
- 150 mm diameter
- 62 mm height
- $7 \pm 0.5$  % air voids

### Criteria

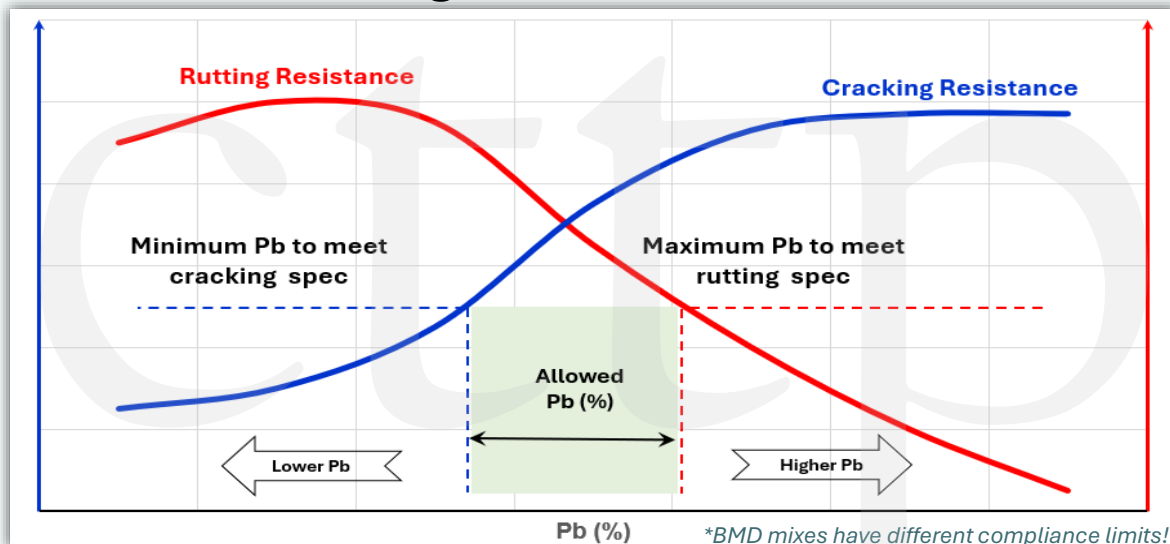
- Minimum CT Index = **75**



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## Balanced Mix Design



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## Mix Design Verification

Mix designs no longer have an expiration date.

A mix design that has not been used on an ARDOT project for the last 2 years is **INACTIVE**.

Mix designs with an expiration date may remain in production if they are not inactive.

A passing field verification may be submitted to Materials Division to be reactivated.



SS-400-4

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## Mix Design Verification

Required at the start of mix production or after an interruption of more than 120 days

Plant set up

- Mix Design Cold Feed %
- Optimum % Binder

Verify

- % Binder
- Gradation
- % Air Voids
- % VMA



SS-400-4

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## Verification Attempts

- 2 attempts allowed on ARDOT project
- 3 attempts allowed on non-ARDOT project

Max of 200 tons placed on ARDOT projects

Asphalt Content may not be changed until after verification of the mix design



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## Mix Verification on ARDOT Project

### If 1<sup>st</sup> attempt doesn't verify

Adjustments can ONLY be made to aggregate proportions

≤ 10 % limit per bin

≤ 20 % limit total adjustment

### If 2<sup>nd</sup> attempt doesn't verify

New mix design required



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## After Successful Verification

Binder content shall be adjusted to obtain optimum binder content on mix design

Binder content shall never be adjusted to lower than design value

Can not make changes to binder content for control of a volumetric property

All binder content changes must be reported to the Engineer in advance

Contractor is allowed a 1-time field mix design



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## HMA Applications

**cttp**  
Center for Training  
Transportation Professionals

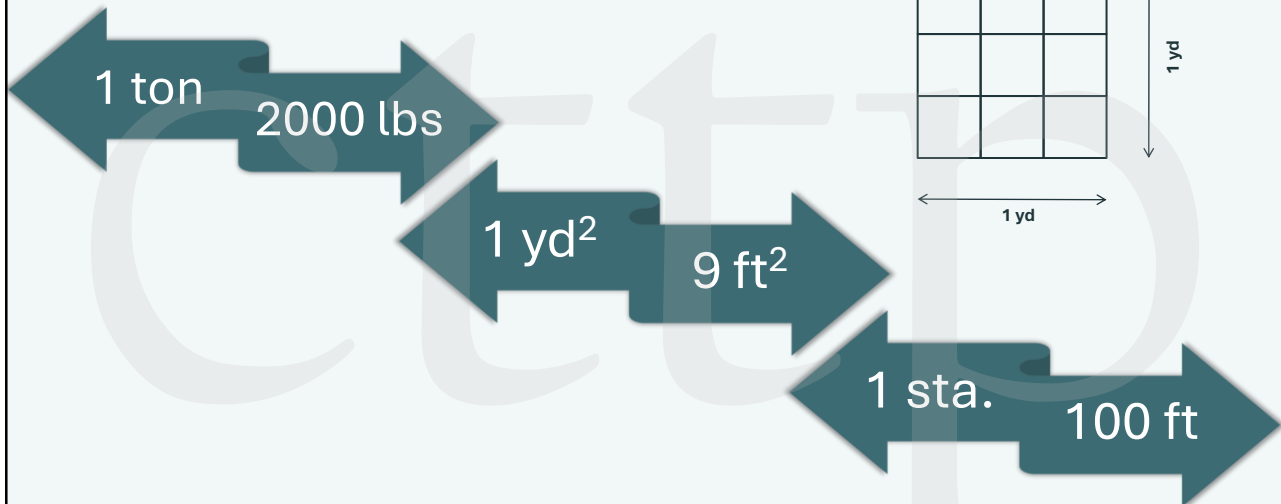


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## Conversions



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## Stations

### Station 50 + 80

- 50 stations + 80 feet
- $(50 \times 100) + 80$  feet
- 5080 feet from start



### Find the distance (ft) between station 17 + 35 and 25 + 79

- Drop "+" sign to convert distance to feet

$$\begin{array}{r} 2579 \text{ ft} \\ - 1735 \text{ ft} \\ \hline 844 \text{ ft} \end{array}$$

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## Application Rate

Describes the weight of asphalt needed to cover an area to produce the required thickness of pavement

- Checking the application rate ensures that the proper amount of asphalt is applied to the roadway

Application Rate (lb/yd<sup>2</sup>)

Weight (lb) = (tons)(2,000)

$$\text{Area (yd}^2\text{)} = \frac{(\text{length})(\text{width})}{9}$$

$$\text{Rate} = \frac{(\text{tons})(18,000)}{(\text{length})(\text{width})}$$

*Length and width measured in feet*

79

79

## Application Rate

Find the application rate in lb/yd<sup>2</sup> for 700 tons of asphalt placed in an area 12' wide by 4774' long.

$$\text{Rate} = \frac{(\text{tons})(18,000)}{(\text{length})(\text{width})}$$

$$\frac{(700)(18,000)}{(4,774)(12)} = \frac{12,600,000}{57,288} = 219.94...$$

**220 lb/yd<sup>2</sup>**

80

80

## Application Rate

Find the application rate in lb/yd<sup>2</sup> for 1000 tons of asphalt placed from station 62 + 20 to station 101 + 67 and 16' wide

$$\text{Rate} = \frac{(\text{tons})(18,000)}{(\text{length})(\text{width})}$$

81

81

## Quantity of Asphalt

The weight of asphalt mixture required to cover an area to a prescribed depth or application rate

- A typical assumption is that it takes approximately 110 pounds of asphalt mixture per square yard to produce a compacted pavement one inch thick

$$\text{Tons} = \frac{(\text{Rate})(\text{length})(\text{width})}{(18,000)}$$

$$\text{Weight (tons)} = \frac{(\text{Rate})(\text{Area})}{2000}$$

*Rate measured in lb/yd<sup>2</sup>*

$$\text{Area (yd}^2\text{)} = \frac{(\text{length})(\text{width})}{9}$$

*Length and width measured in feet*

83

83

## Quantity of Asphalt

Find the tons of asphalt needed to pave a 10 ft wide, 300 ft long drive with an application rate of 220 lb/yd<sup>2</sup>

$$\text{Tons} = \frac{(\text{Rate})(\text{length})(\text{width})}{(18,000)}$$

$$\text{Tons} = \frac{(220)(300)(10)}{(18,000)} = \frac{660,000}{18,000} = 36.66\ldots$$

**37 tons**

84

84

## Quantity of Asphalt

Find the tons of asphalt needed to pave a 50' wide x 300' parking lot with an application rate of 160 lb/yd<sup>2</sup>

$$\text{Tons} = \frac{(\text{Rate})(\text{length})(\text{width})}{(18,000)}$$

85

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# ARDOT Specifications

## Standard Specifications & Errata

- Mix design and quality control requirements

## Supplemental Specifications

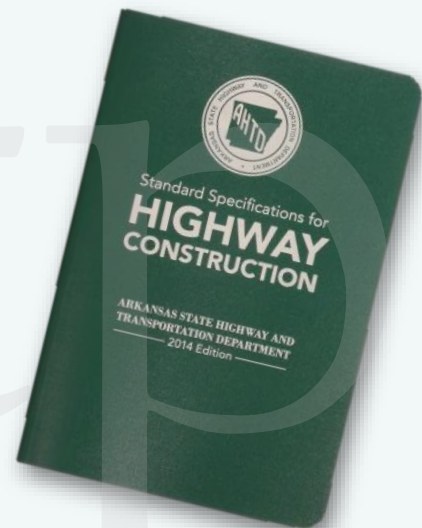
- Changes to the Standard Specifications

## Job Plans

- Mix design requirements and application rates

## Special Provisions – Apply only to individual jobs

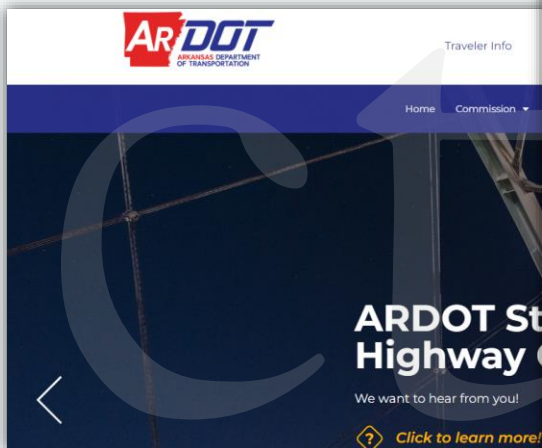
- Recycled Asphalt Shingles
- Warm Mix Asphalt
- PWL
- Joint Densities



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# ARDOT Publications



Environmental Studies	Home / Publications / Manuals
Funnel Chart	<b>Manuals</b>
Highway Tourist	AASHTO SDMS Getting Started Manual
Highway Safety	AASHTO SDMS Technical Data Guide
Historic Bridges	Access Driveway Regulations
Institutional Road	Arkansas Bicycle Guide
Manuals	Arkansas Drivers Manual
Motor Vehicle an	Contractor Compliance Manual
Performance an	Design-Build Guidelines and Procedures
Policy on Highw	Design-Build Contract Rules
Public Involvem	Erosion and Sediment Control Design and Construction Manual
Public Transport	Instruction Manual for Federal Transit Administration (FTA) Vehicles (Section 5310)
Public Transport	Local Government Procedures for Compliance with the National Bridge Inspection Standards
Public Transport	Manual of Field Sampling and Testing Procedures
Public Transport	Procedures for New or Revised Freeway Access in Arkansas
Research Inform	Right of Way Appraisal Operational Manual
Risk-Based Trans	Right of Way Policies and Procedures Manual
Selected Facts a	Roadway Design Drainage Manual
Standard Specifi	Roadway Design Plan Development Guidelines
State Freight Pla	Safety Manual
Statewide Bicycl	Statewide Stormwater Management Plan
Statewide Long	Stewardship and Oversight Agreement – April 2015
State Planning a	Survey Manual
State Safety Ove	
State Safety Ove	
Stewardship and	
Stormwater Pub	
Strategic Highw	
Strategic Plan	

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## Field Compliance Limits (ARDOT Table 410 – 1)

Property		Tolerance	
Binder Content		± 0.3% (mix design)	
Air Voids		2.5% - 4.5%	2025
VMA	37.5 mm	11.0% - 13.5%	
	25.0 mm	12.0% - 14.5%	
	12.5 mm	14.0% - 16.5%	
	9.5 mm	15.0% - 17.5%	
Gradation	See ARDOT Section 404.04		
Field Density	92.0% - 97.0% or 90.0% - 97.0%		2025

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## Field Compliance Limits (ARDOT 404.04)

ARDOT Gradation	Sieve Size		Tolerance
<i>Tolerances are applied to the Job Mix Formula (JMF)</i>	1"	25.0 mm	± 7.0 %
	¾"	19.0 mm	± 7.0 %
	½"	12.5 mm	± 7.0 %
	#4	4.75 mm	± 7.0 %
	#8	2.36 mm	± 7.0 %
	#16	1.18 mm	± 4.0 %
	#30	0.60 mm	± 4.0 %
	#50	0.30 mm	± 4.0 %
	#100	0.15 mm	± 4.0 %

90

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# Specification Limits

ARDOT specification limits are absolute!

Observed or calculated values are not rounded for determination of compliance

- Compared directly with the limit
- Average values are rounded to same number of significant digits

Any deviation outside limits is considered non-compliance

- Failing test

91

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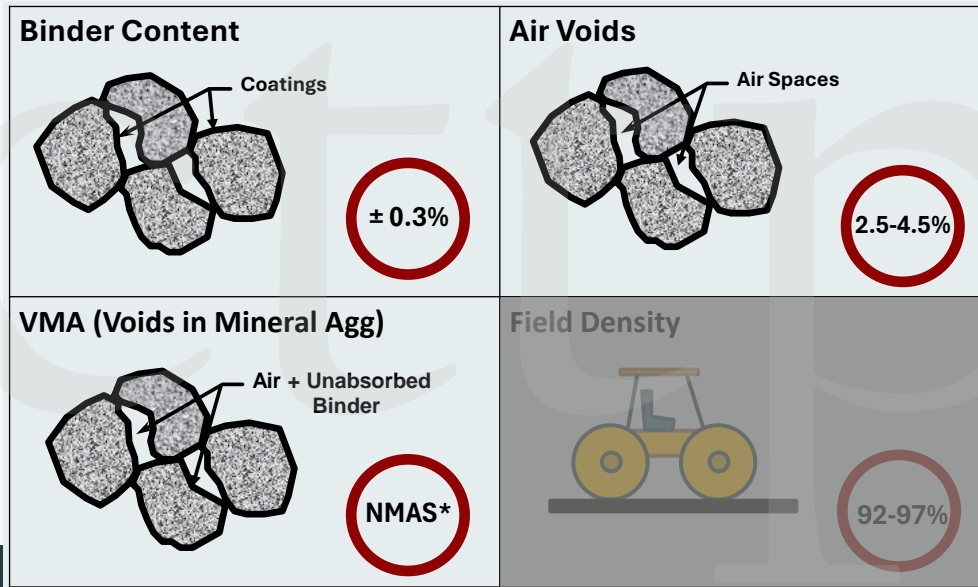
# Submittals - SiteManager



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## Prepare Samples for QC/QA Testing



93

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## Quality Control / Quality Assurance

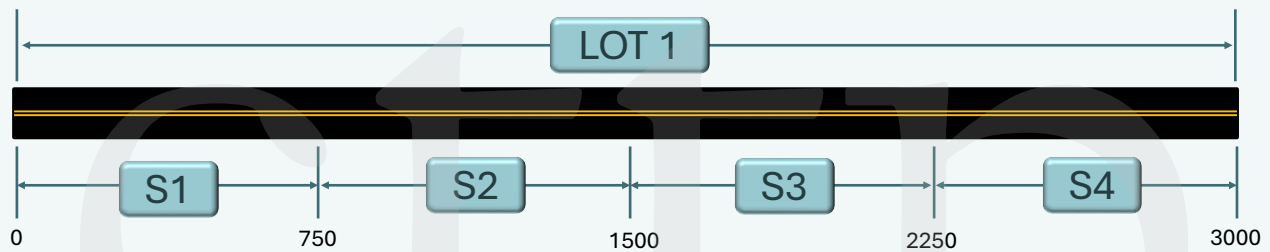


94

94



## Random Sampling - Tonnage



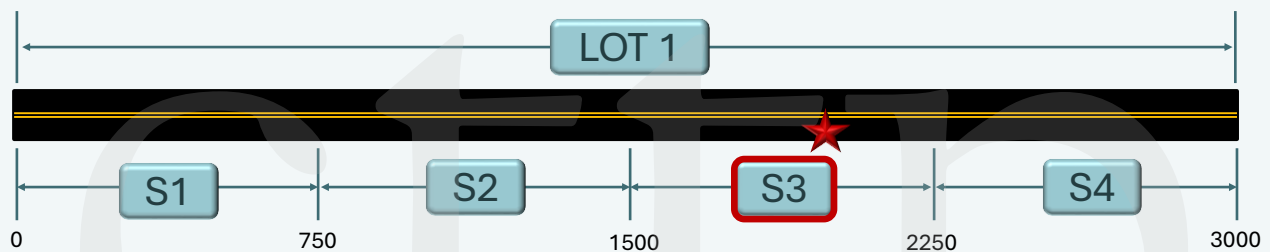
Step 1: Multiply random number (RN) by lot or subplot size

Step 2: Add previous tonnage

95

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## Random Sampling - Tonnage



Example: Lot 1, Sublot 3, RN = 0.64

$$750 \times 0.64 = 480$$

$$480 + 1500 = 1980$$

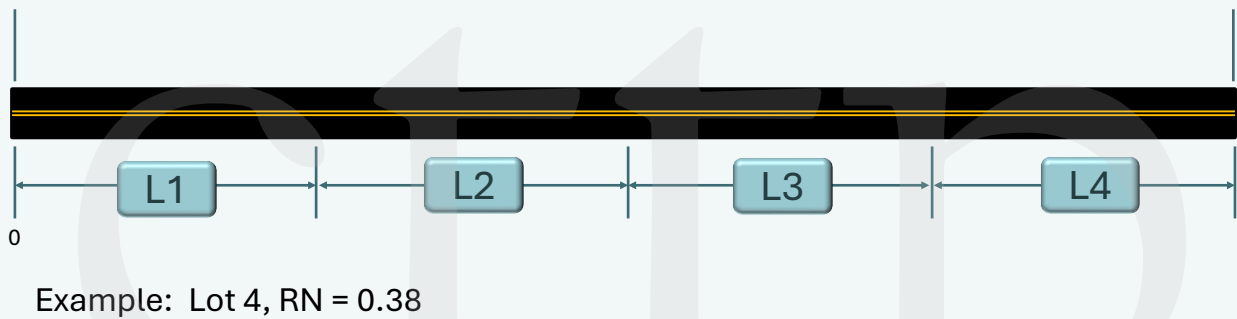
**1980**



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## Random Sampling - Tonnage



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## Sampling Bituminous Mixtures

AASHTO R 97

**cttp**  
Center for Training  
Transportation Professionals



100

100

## ARDOT Specifications

ARDOT 404.04 – Sampling shall be performed according to AASHTO R 97 and ARDOT 465

- Note 1: Samples shall be taken from trucks at the plant



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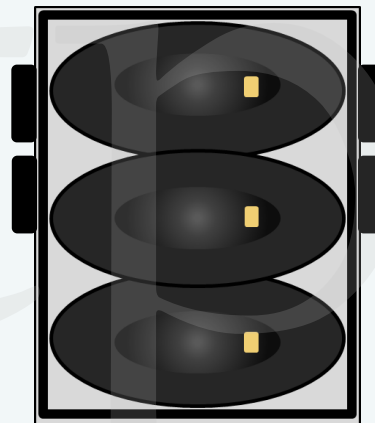
## Transport Units

Visually divide truck bed into 3 or 4 equal sections

Remove 6-12" of topmost material

Obtain 1 portion from each section

Combine portions



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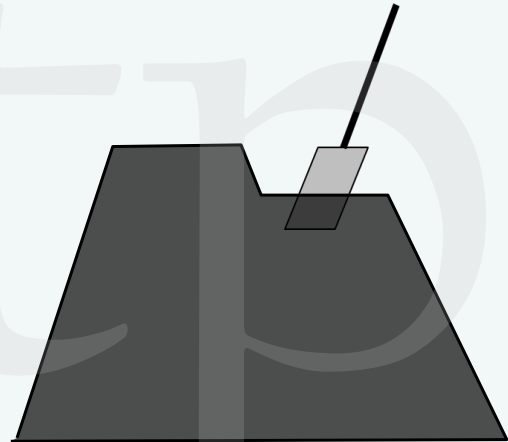
## Transport Units

Avoid loss of larger aggregates from overfilling shovel

Avoid buildup of fines on shovel

Sample should look like the load sampled!

If not, get another sample from the same truck!



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## Windrow Sampling

Visually divide the windrow unit into 3 approximately equal sections

- Avoid sampling in the beginning or end of a windrow unit
- Choose a sample location in each section



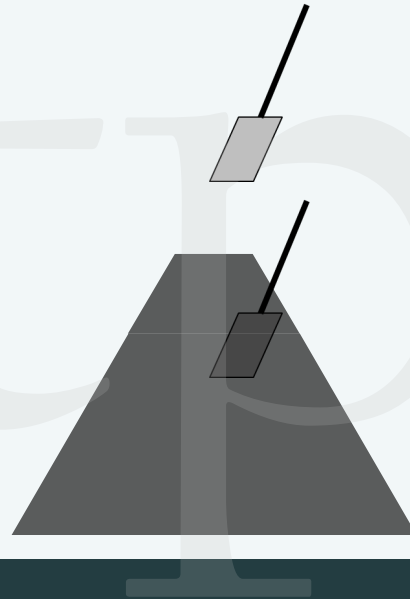
104

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## Windrow Sampling

### Sample portions

- At each sample location, discard the top foot of windrow
- Fully insert shovel into the exposed surface
  - Vertically
- Roll back shovel and lift material
- Avoid material rolling off shovel
- Combine portions



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## Other Sampling Locations

### Roadway (before compaction)

- Take samples behind paver, but in front of breakdown roller
- “Cookie Cutter”
- Plate

Used when asphalt is placed on grade or base material

### Paver or MTD Hopper

- Remove top 6 – 10 inches of asphalt
  - Take sample from center of hopper
- Stay at least 1.5' away from sides

### Stockpiles

- Remove top 4 inches of asphalt

*Always obtain a minimum of 3 portions*

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# Transportation

## Protect the sample

- Avoid contamination
- Prevent loss of material
- Maintain temperature



## Labeling

- Job number
- Source of sample
  - Plant / mix design number
- Sample location
  - Tons
  - Lot / subplot



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# Reducing Samples of HMA to Testing Size

AASHTO R 47

**cttp**  
Center for Training  
Transportation Professionals

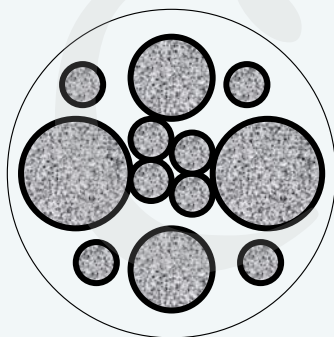


108

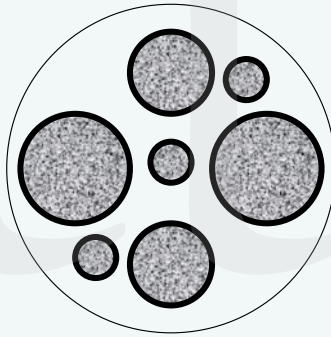
108

## Reducing Samples

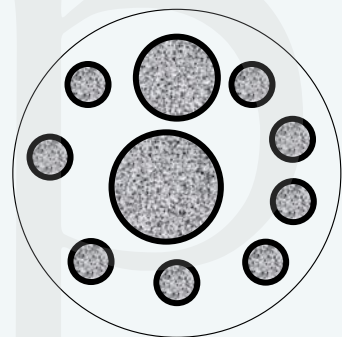
Methods used to reduce samples in size while maintaining physical characteristics and size proportions



Original



Coarse



Fine

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## Reducing Samples

Gradation of a reduced HMA sample affects its volumetric properties

- Pb
- Gmm
- % Air Voids
- % VMA
- % Density

Sieve	Design	Coarse	Fine
3/4"	100	100	100
1/2"	92	89	95
3/8"	81	78	84
# 4	52	49	55
# 8	30	27	33
# 16	20	17	23
# 30	16	15	18
# 50	13	11	15
# 100	9	8	10
# 200	5.2	4.2	6.2
<b>Pb</b>	<b>5.5 %</b>	<b>4.75 %</b>	<b>6.27 %</b>

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# Reducing Samples

## Maintain Temperature

- Heat equipment up to maximum mixing temperature

## Release Agents

- May be used to lightly coat equipment surfaces
  - Use only approved release agents
  - No solvents or petroleum-based products

## Methods

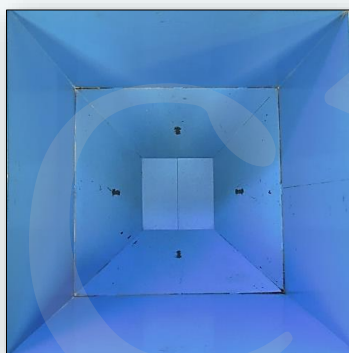
- Mechanical Splitter
  - Recommended for large samples
  - Type A
  - Type B
- Quartering Method
  - Sectoring
- Incremental Method

2023

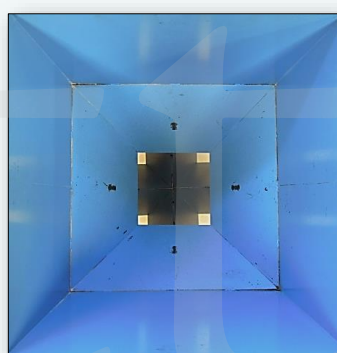
111

111

## Type A Mechanical Splitter



Fill the hopper



Open the hopper

Collect diagonally opposite quarters



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## Type B Mechanical Splitter

Fill hopper or pan

- Evenly distribute

Open hopper at a controlled rate

Collect one side



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## Quartering

Straight Edge

Quartering Template

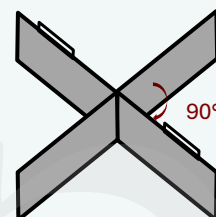
Place on nonstick surface

Mix well – turn pile 4+ times

Form conical pile and flatten

Separate into quarters using straightedge or template

Collect diagonally opposite quarters



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## Sectoring

After Quartering:

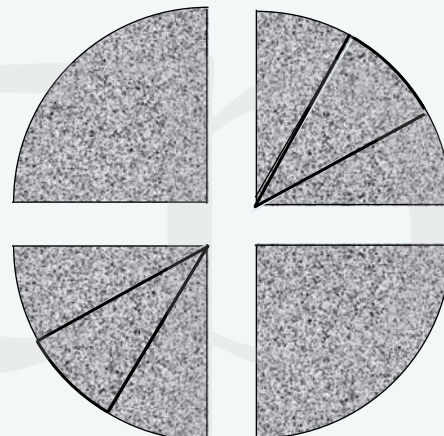
Use a straightedge to obtain a sector

- Sector is from center to outer edge, “pie” slice

Drag sector away from quarter

Obtain equal size sector from the diagonally opposite quarter

Combine sectors



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## Incremental Method

Place sample on nonstick paper

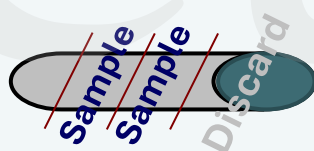
- Mix well – turn pile 4+ times

Roll asphalt into cylindrical loaf

- Discard end quarter of loaf

Cut off (collect) desired sample sizes

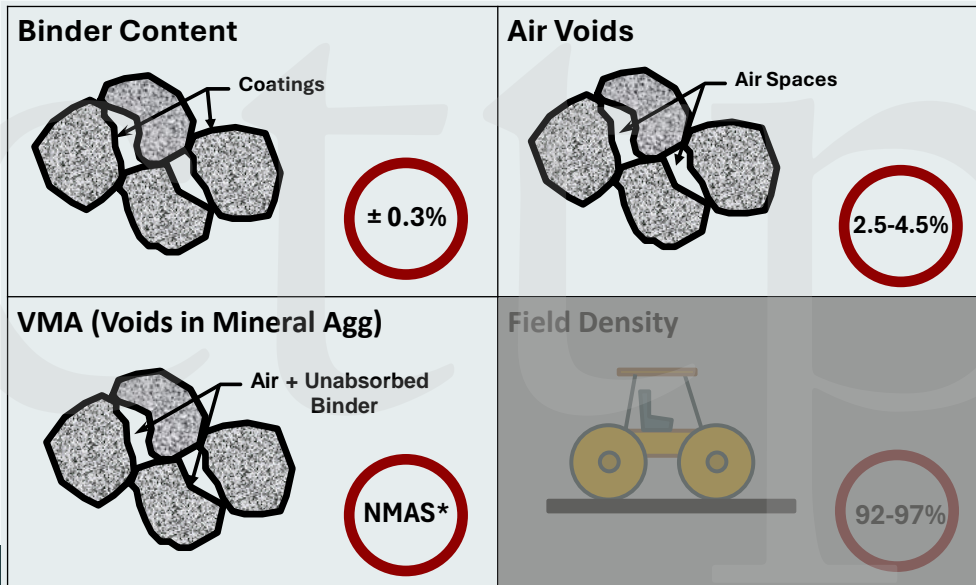
- Remix and repeat as necessary



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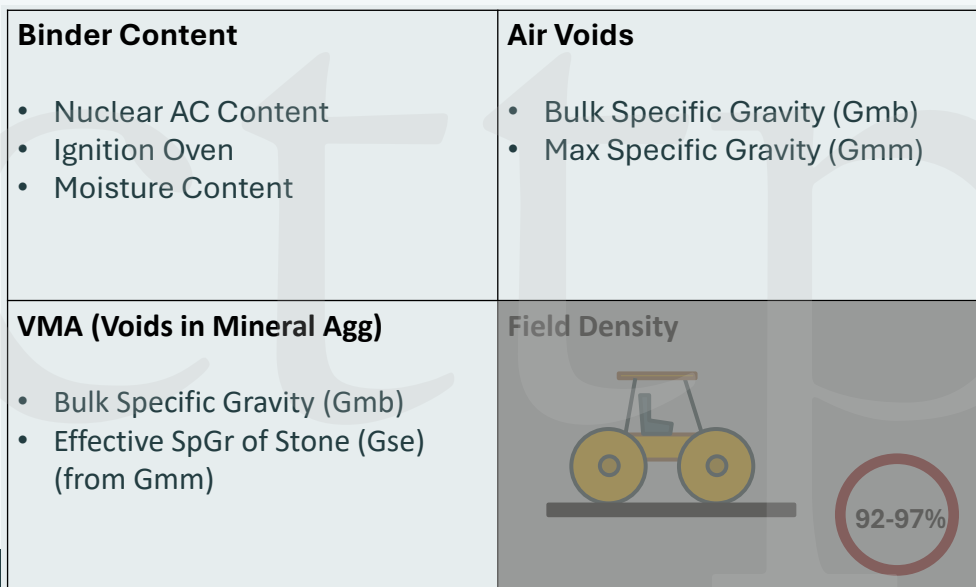
## Prepare Samples for QC/QA Testing



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## Prepare Samples for QC/QA Testing



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# Preparing HMA Specimens by Gyratory Compactor

AASHTO T 312



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## Gyratory Compaction - Equipment

Gyratory compactor

- Mold
- Bottom
- Top

Oven

- Compaction temperature
- $\pm 5^{\circ}\text{F}$

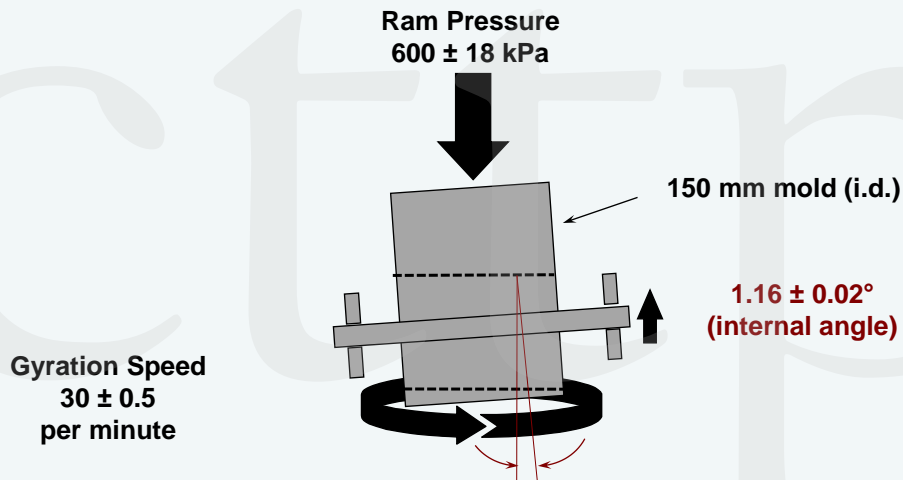
Thermometer



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## Gyratory Compactor Parameters



121

## Compactor Preparation

Verify settings

- Angle & pressure
- Number of gyrations
  - Ndes shown on mix design

Lubricate bearing surfaces

Preheat molds and plates to compaction temperature

- At least 30 minutes
- Reheat at least 5 minutes between uses



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## Preparation

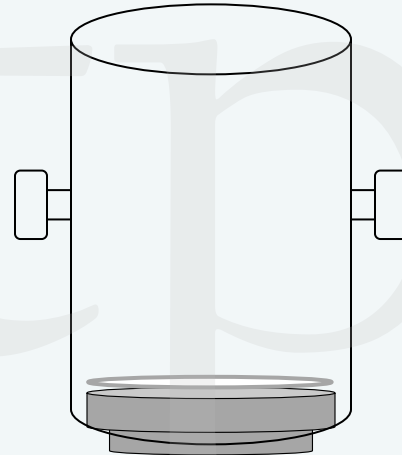
### Reduce sample

- $115 \pm 5$  mm height
- (4400 g – 4800 g)

### Bring asphalt mixture to compaction temperature

### Assemble mold

- Largest side of plate goes toward specimen
- Paper disk



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## Procedure

### Place asphalt mixture into mold in one lift

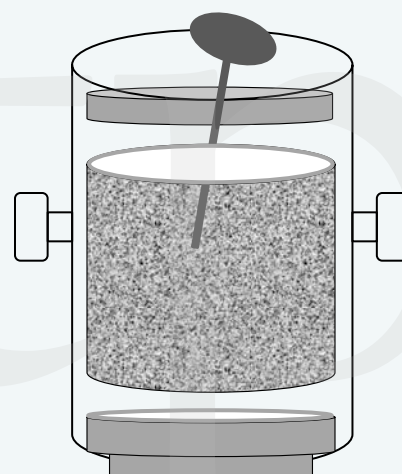
- Avoid segregation
- Level surface of HMA

### Verify temperature

- Compaction temperature shown on mix design

### Insert paper disk

### Place top plate in mold if necessary



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## Gyratory Compaction Procedure

- Load mold into compactor
- Compact specimen
- Remove mold from compactor



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## Gyratory Compaction Procedure

- Extrude specimen from mold
  - Cool tender specimens
  - Extrude slowly
- Remove paper disks
- Cool to room temperature
  - Compact at least 2 specimens



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## Mold Diameter Verification

### Frequency

- Yearly or 80 hours

### Verify inside dimensions

- 3-point bore gauge
- Calibrated master ring

### Mold temperature

- 64 – 82 °F



### Procedure

- Record 3 measurements at each height
  - 50 mm from wear end
  - 100 mm from wear end
  - 50 mm from opposite end

***In-service mold diameters must be  $\leq 150.2$  mm***

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## Gyratory Compactor Verification

### Frequency

- Follow mfr. recommendations
- 12 month maximum

### Verify

- Internal angle
- Pressure
- Rotation speed
- Height measurement

### Additional Checks

- Change in location
- Repairs affecting calibration

### Optional Check

- New season of mix designs

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## Bulk Specific Gravity of Compacted HMA Specimens

AASHTO T 166



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## Bulk Specific Gravity

Used to determine the volumetric properties of compacted mix

- Gyrotory specimens or cores



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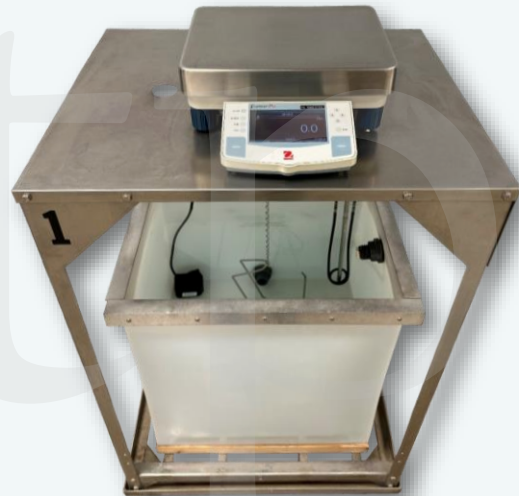
## Bulk Specific Gravity - Equipment

### Scale

- Readable to at least 0.1 % of sample mass
- Suspension apparatus (weigh-below)

### Water bath

- Overflow device to maintain constant water level
- $77 \pm 2^\circ\text{F}$
- Agitator and heater (optional)



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## Bulk Specific Gravity – Method A

Remove any foreign material

Dry specimen to constant mass

2024

- $126 \pm 5^\circ\text{F}$
- Vacuum ( $\geq 2$  cycles)

Cool to  $77 \pm 9^\circ\text{F}$



Weigh specimen and record dry mass in air



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## Bulk Specific Gravity – Method A

Prepare water bath

- Fill and allow to stabilize
- Tare out suspension apparatus

Submerge specimen in water bath

- Leave submerged for  $4 \pm 1$  minutes

 Record submerged mass



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## Bulk Specific Gravity – Method A

Remove specimen from water bath  
Quickly bring to SSD with damp  
towel

- 15 seconds



Weigh specimen and record SSD  
mass 



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## Calculation of $G_{mb}$ and Absorption

$$G_{mb} = \frac{A}{(B - C)} \quad \% \text{ Abs} = \frac{(B - A)}{(B - C)} \times 100 \%$$

A = Dry mass of specimen

B = SSD mass of specimen

C = Submerged mass of specimen

*Report  $G_{mb}$  to 0.001, Abs to 0.01%*

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## Bulk Specific Gravity – Method C (Rapid Test)

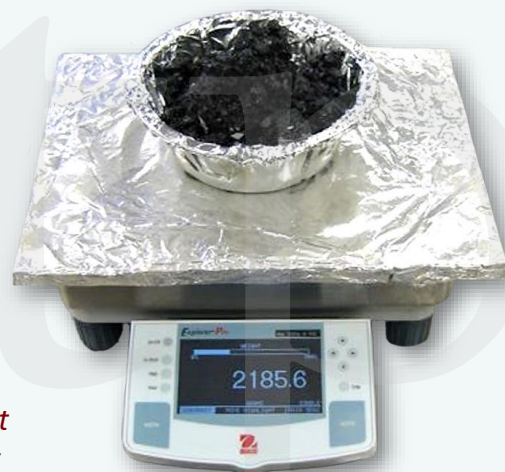
Obtain submerged mass

Obtain SSD mass

Dry specimen at  $230 \pm 9^\circ\text{F}$  to  
constant mass

Cool to room temperature

Obtain dry mass



*This method destroys the specimen but  
allows cores to be tested the same day*

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## % Absorption Requirements

AASHTO T 166 is only applicable for samples that absorb 2 % or less water by volume

- If > 2 % absorption, rerun test
  - Dry to constant mass
  - AASHTO T 275 (Paraffin Coating)
  - AASHTO T 331 (Vacuum Sealing)

ARDOT Special Provision

- Longitudinal Joint Densities

***Joint densities are susceptible to having more than 2 % absorption***

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## Theoretical Maximum Specific Gravity

AASHTO T 209

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## The Rice Test (Gmm)

Influenced by the mixture

- Binder
- Stone
- Moisture

Influences pay

- % Air Voids
- % VMA
- % Density



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## Rice Test Equipment

Vacuum System



Water Bath & Scales



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## Sample Preparation

### Plant-produced samples

- May be short-term conditioned at  $135 \pm 3^\circ\text{C}$  ( $275 \pm 5^\circ\text{F}$ )
- Reduce samples to meet minimum size requirements

### While still warm, separate sample

- $\leq \frac{1}{4}"$  in size (no fine clumps)
- Prevents trapped air between particles

### Cool to room temperature



### Sample Size

NMAS	Sample Size (minimum)
$\geq 37.5$ mm	4000 g
19 – 25 mm	2500 g
$\leq 12.5$ mm	1500 g

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## Rice Test Procedure

Tare bowl on the scale or record an empty mass

Place sample into vacuum bowl



Weigh vacuum bowl with sample

 Record net mass of sample



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## Rice Test Procedure

Add 77 ° F water to completely cover the sample

- Sink floating particles
- Optional: Add 5-10 mL of diluted wetting agent
  - Aerosol OT



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## Rice Test Procedure

Remove trapped air by applying vacuum

- 2023 •  $30 \pm 5$  mm Hg ( $4.0 \pm 0.6$  kPa)
- 2022 •  $15 \pm 1$  minutes

Agitate vacuum bowl

- Mechanical shaker
- Vigorously shake every 2 minutes



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## Rice Test Procedure

Turn off table, pump, etc.

Release vacuum slowly

- $\leq 60 \text{ mm Hg/s}$  (8 kPa/s)
- $\sim 12$  seconds

Prepare water bath

- Fill to overflowing
- Allow water level to stabilize
- Tare suspension apparatus




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## Rice Test Procedure

Submerge vacuum bowl + sample

- $77 \pm 2^\circ \text{F}$
- $10 \pm 1$  minutes

 Record submerged mass of bowl + sample

Remove bowl from water bath

 Record standardized mass of vacuum bowl



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## Calculation of Gmm

$$G_{mm} = \frac{A}{(A - C)}$$

A = Dry mass of sample

C = Submerged mass of sample

$$C = (\text{bowl} + \text{sample})_{\text{sub}} - (\text{bowl})_{\text{sub}}$$

*Report all specific gravities to the nearest 0.001*

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## Standardized Bowl Mass

Prepare water bath

Submerge empty vacuum bowl

- $77 \pm 2$  °F
- $10 \pm 1$  minutes



Record submerged mass of bowl

- Repeat 2 more times (3 total)
- **If within 0.3 g**, average 3 masses



Record average mass



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## Bulk Specific Gravity of Compacted Asphalt Mixtures Using Paraffin- Coated Specimens

AASHTO T 275



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## Paraffin Coating - Equipment

### Scale

- Readable to 0.1 % of sample mass or better

### Suspension Apparatus

### Water Bath

- Overflow device to maintain constant water level
- $77 \pm 0.9^\circ\text{F}$
- Agitator and heater (optional)

### Drying Apparatus

- Oven at  $125 \pm 5^\circ\text{F}$
- Vacuum dryer

Crock pot or other suitable device  
for heating paraffin wax



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## Paraffin Coating - Procedure

Obtain the specific gravity of the paraffin at  $77 \pm 1.8^\circ\text{F}$

- Manufacturer
- Approximately 0.915

Heat paraffin to about  $10^\circ\text{F}$  above its melting point

- $120 - 150^\circ\text{F}$

Dry specimen to constant mass

- $125 \pm 5^\circ\text{F}$
- Vacuum ( $\geq 2$  cycles)

Cool to  $77 \pm 9^\circ\text{F}$



Weigh specimen and record dry mass in air

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## Paraffin Coating - Procedure

Coat specimen on all sides with melted paraffin

Seal surface voids


Cool at  $77 \pm 9^\circ\text{F}$  for at least 30 minutes



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## Paraffin Coating - Procedure


-  Weigh specimen and record coated mass in air



Prepare water bath

- Fill to overflowing
- Allow water level to stabilize
- Tare suspension apparatus

Submerge coated specimen in water bath for **4 ± 1 minutes**

-  Record submerged mass

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## Paraffin Coating – Calculation

$$G_{mb} = \frac{A}{D - E - \left(\frac{D - A}{F}\right)}$$

A = Dry mass of specimen

D = Mass of coated specimen

E = Submerged mass of coated specimen

F = Specific gravity of paraffin at 77 °F

*Report  $G_{mb}$  to 0.001*

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## Bulk Specific Gravity of Compacted Asphalt Mixtures Using Automatic Vacuum Sealing

AASHTO T 331



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## Vacuum Sealing - Equipment

### Scale

- Readable to 0.1 % of sample mass or better
- Suspension apparatus

### Water bath

- Overflow device to maintain constant water level
- $77 \pm 0.9^{\circ}\text{F}$
- Agitator and heater (optional)

### Drying apparatus

- Oven or vacuum

### Vacuum Chamber

- Reach 5 mm Hg in 60 seconds

### Plastic sealing bags

- Thickness of 0.005 – 0.007 inch
- 14.5 – 15.5 inch opening



### Cushioned sliding plate

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## Vacuum Sealing - Procedure

✎ Record bag correction factor

- Apparent specific gravity of bag
  - Manufacturer

Dry specimen to constant mass

- $125 \pm 5$  °F
- Vacuum ( $\geq 2$  cycles)

Cool to  $77 \pm 9$  °F

✎ Weigh specimen and record dry mass in air

✎ Inspect sealing bag for holes, weigh and record bag mass

Place bag on sliding plate inside vacuum chamber

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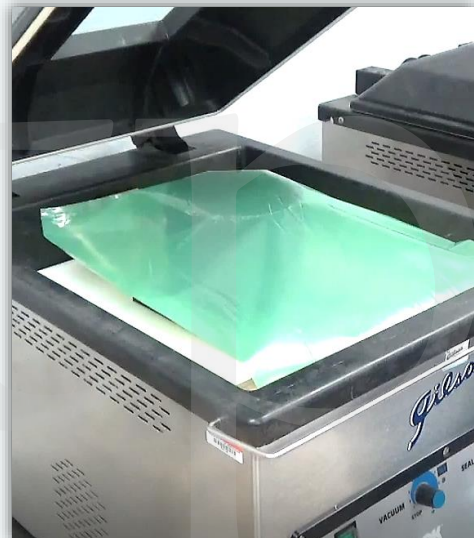
## Vacuum Sealing - Procedure

Center specimen inside bag and on top of sliding plate

- Place smoothest side down

Place bag across seal bar

- Smooth out wrinkles
- Leave about 1 inch of overhang



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## Vacuum Sealing - Procedure

### Seal specimen

- Close lid and latch
- Wait for lid to open



### Inspect bag and seal

- Repeat with new bag if loose or leak is noted

Within 60 seconds, submerge sealed specimen in water bath

Ensure bag is not touching sides of water bath

- Remove trapped pockets of air

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## Vacuum Sealing - Procedure

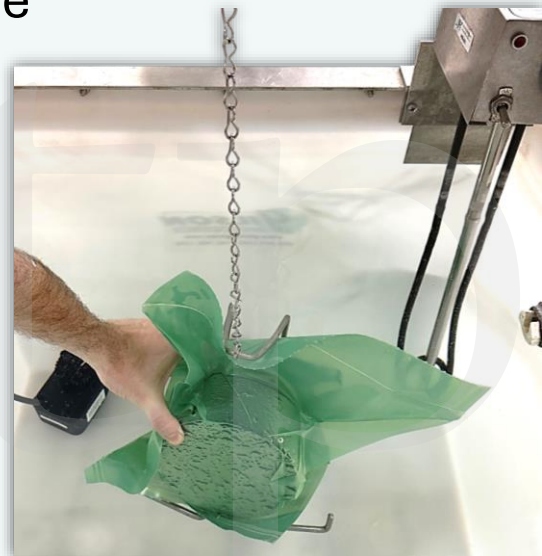
Record submerged mass of sealed specimen

Remove sample from water bath

Cut open bag

Record final weight of sample in air

- Limited to 0.08 % loss or 0.04 % gain in weight



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## Vacuum Sealing – Calculation

$$G_{mb} = \frac{A}{C + B - E - \left(\frac{B}{F}\right)}$$

A = Initial dry mass of specimen

B = Mass of the bag

C = Final mass of specimen

E = Submerged mass of sealed specimen

F = Bag correction factor (apparent specific gravity)

*Report  $G_{mb}$  to 0.001*

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## Vacuum Sealing - Calibration

### Vacuum chamber

- Verify vacuum using vacuum gauge
  - Every 3 months
  - After repairs
  - After relocation

### Vacuum gauge

- Range of at least 0 – 10 mm Hg
- Must allow placement inside chamber



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# Moisture Content of Asphalt Mixtures by Oven Method

AASHTO T 329

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## Moisture Content - Equipment

### Oven

- Mixing temperature or
- $325 \pm 25$  °F

### Scale

- Readable to at least 0.1 g
- $\geq 2$  kg capacity

### Thermometer


- 2022 → • Accurate to  $\pm 3.6$  °F ( $\pm 2$  °C)



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## Moisture Content – Procedure


 Record empty mass of sample pan

- Include weight of liners

Place asphalt mixture in pan

 Measure and record temperature of the mix

- Distribute sample evenly in container

 Record mass of sample pan and moist test sample

- Determine initial mass of sample

Dry sample for  $90 \pm 5$  minutes

- Determine mass of sample

Continue drying until  $\leq 0.05\%$  change in mass

- Check at  $30 \pm 5$  min. intervals

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## Moisture Content – Calculation

$$\% \text{ Change} = \frac{(M_p - M_n)}{M_n} \times 100$$

*$M_p$  – mass of previous measurement*  
 *$M_n$  – mass of newest measurement*

Cool to roughly the same temperature as initially recorded

 Weigh and record mass of sample pan and dry test sample

- Determine final dry mass of sample

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## Finding Constant Mass

1245.6 g

- Initial “wet” mass

1244.4 g

- 0.096 % change

*More drying needed*

1244.1 g

- 0.024 % change – final “dry” mass

*<0.05, constant mass*

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## Calculation

$$\% \text{ MC} = \frac{(M_i - M_f)}{M_f} \times 100 = \frac{(W - D)}{D} \times 100$$

$M_i$  = Initial mass of asphalt mixture (wet)

$M_f$  = Final mass of asphalt mixture (dry)

*Subtract tare weight of pan to get mixture weights!*

*Report moisture content to the nearest 0.01 %*

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## Moisture Content – Calculation

Tare Weight = 356.8

Wet + Tare = 1355.7

Dry + Tare = 1354.8

$W = 1355.7 - 356.8 = \mathbf{998.9}$

$D = 1354.8 - 356.8 = \mathbf{998.0}$

$$\% \text{ MC} = \frac{(W - D)}{D} \times 100$$

$$= \frac{(998.9 - 998.0)}{998.0} \times 100$$

= 0.09018...

**0.09 %**

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## Moisture Content – Calculation

Tare Weight = 243.8

Wet + Tare = 1505.7

Dry + Tare = 1505.2

$$\% \text{ MC} = \frac{(W - D)}{D} \times 100$$

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# Determination of Asphalt Content by the Nuclear Method

ARDOT 449



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## Gauge Preparation

Place at least 30 feet from other sources of radiation

Keep area clear of hydrogenous materials

- Water
- Plastics
- Asphalt

Make sure chamber is clean and empty

Turn on gauge / warm up

Perform an 8 or 16 minute background count

- Daily or whenever gauge surroundings have changed

Record background count in a daily log

- Verify new background is within  $\pm 1\%$  of previous background count

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## Gauge Preparation

Activate the appropriate calibration

Set AC gauge test time for field testing

- 4, 8, or 16 minutes

Obtain a representative portion of asphalt mixture

- AASHTO R 97

Tare sample pan on scale or record empty weight



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## AC Gauge Field Testing

Place asphalt mixture in sample pan

- 2 lifts
  - Lightly tamp each lift
- Match calibration weight within  $\pm 5$  grams
- Level asphalt
  - Press down on leveling plate until asphalt surface is flush with top rim of pan
- Verify weight



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## AC Gauge Field Testing

Measure temperature

- Within  $\pm 10$  °F of calibration temp

Load sample pan into gauge

- Close door

Start test and move away 3 ft



Record counts and % AC (Pb)

- Average multiple tests



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## AC Gauge Field Testing

Determine moisture content AASHTO T 329 to the nearest 0.01 %

- Subtract reported moisture content from the AC gauge test result
- Round and report binder content to the nearest 0.1 %

*Report binder content to  
the nearest 0.1% !*

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## Asphalt Content by Nuclear Gauge

Pb from mix design = 4.1%

Pb measured by AC Gauge = 3.96 %

Moisture Content = 0.04 %

$$P_b = 3.96 - 0.04 = 3.92$$

**3.9 %**

*Report  $P_b$  to the nearest 0.1 %*

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## Asphalt Content by Nuclear Gauge

Pb from mix design = 4.1%

Pb measured by AC Gauge = 4.07 %

Moisture Content = 0.05 %

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# Calibration of Asphalt Content Gauge Troxler 3241-C

ARDOT 449A

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## AC Gauge Calibration

AC gauge measures “counts”  
Calibration converts counts to Pb

### Calibrations

- Gauge specific
- Mix design specific
- Should be done at the expected location of testing



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## AC Gauge Calibration Equipment

AC Gauge

Scale

- Readable to 0.1 g
- Capacity  $\geq 12,000$  g

Sample pan

Leveling plate

- 0.4" metal
- $\frac{1}{2}$ " plexiglass
- $\frac{3}{4}$ " plywood

Thermometer

- 50 – 500 °F



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## Batching Requirements

Number of Points

- 4 batches heated to mixing temperature
- 8000 g of aggregate for each
  - Includes RAP/RAS

Batch weights are based on the mix design



Sieve Size	1	2	3	4	5	Job Mix	Control Points
19	100	100	100	100	100	100	100 %
12.5	74	100	100	100	100	95	90 - 100 %
9.5	47	91	100	100	99	87	90 % Max
4.75	5	21	96	94	80	54	
2.36	3	3	76	65	61	36	28 - 58 %
1.18	3	3	51	43	49	26	
0.6	3	3	32	25	41	18	
0.3	3	3	17	16	32	12	
0.15	2	2	8	14	22	8	
0.075	1.5	1.0	3.5	10.0	12.0	4.6	2 - 10 %
Cold Feed %	20	29	22	15	14		
Gab	2.520	2.616	2.559	2.496	2.544		

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## Determine Calibration Weight

Prepare BLANK sample

- Zero pan on scale or record empty weight

Fill sample pan with the hot, dry, batched aggregate in 2 layers

- 1<sup>st</sup> layer
  - Fill pan about ½ full
  - Tamp aggregate and work corners
  - Drop pan 1" to settle aggregate
- 2<sup>nd</sup> layer
  - Add aggregate until just over full
  - Tamp aggregate and work corners




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## Determine Calibration Weight

Level top surface with straight edge



 Record temperature (200 – 300 °F)

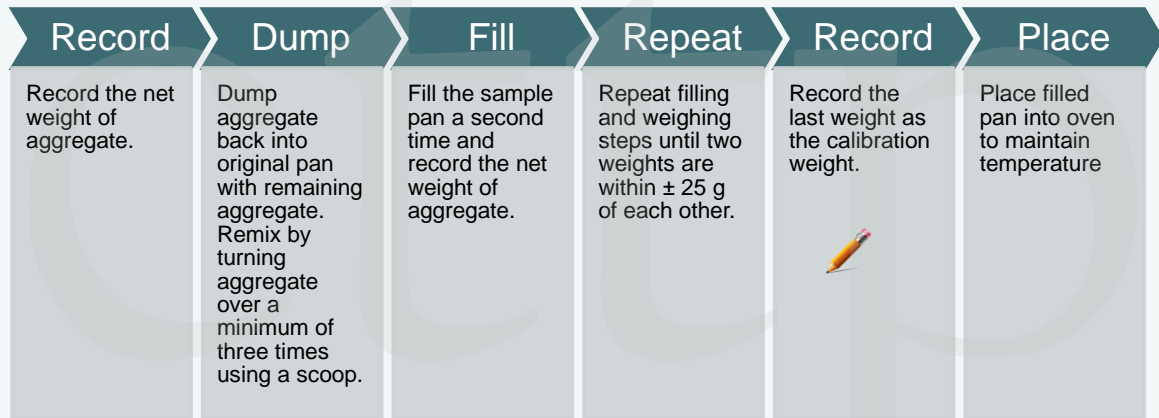
Determine net weight of aggregate to nearest whole gram



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## Determine Calibration Weight



*The calibration weight is used for all remaining samples!*

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## Calibration Samples

3 Required Binder Contents + Blank

- Based on the ARDOT mix design
- After mixing, place samples in oven to maintain temperature

From Mix Design:  
 $Pb_{\text{optimum}} = 4.1 \%$



**Dry**  
0.0 %



**Opt. -1 %**  
3.1 %



**Optimum %**  
4.1 %



**Opt. +1 %**  
5.1 %

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## Calibration Samples

Prepare calibration pans

- Zero pan on scale
- Fill pan in 2 layers
  - Tamp lightly, work corners
  - Slightly overfill
- Match calibration weight within  $\pm 5$  g
- Compress with leveling plate
  - Verify weight
- Bring sample to calibration temp
  - 200 – 300 °F
  - Temp expected during field testing



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## BLANK Sample Counts

Set time to 16 minutes

Load BLANK sample and start test



- Record counts
  - Dry counts may be used to check for changes in aggregate during production



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## AC Gauge Calibration

Start a new calibration

- Three 16-minute counts
- Sample pan
- Gauge derived

Enter calibration weight

- Net weight

Enter the number of asphalt calibration samples

Measure the temperature of the asphalt mixture

 Record calibration temperature



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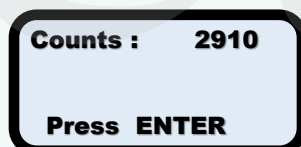
## AC Gauge Calibration

Enter Pb for 1<sup>st</sup> sample

Load pan into gauge

- Start test
- Move away from gauge
  - At least 3 ft

 Record counts



Repeat process for all calibration points



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## AC Gauge Calibration

Record fit coefficient

- Must be at least 0.995

Review input data

- Screen or printer
- Record constants
  - A1, A2, A3

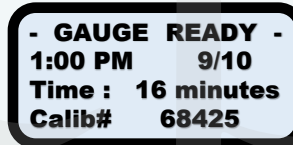
 Record differences if necessary

Activate calibration

Store calibration

- Use mix design number

**Example: HMA 684-25**



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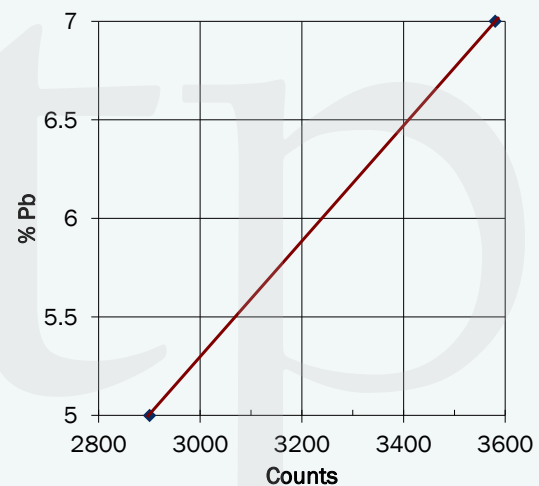
## Fit Coefficient

2 point calibration

% AC	Counts	Difference
5.0	2900	0.000
7.0	3580	0.000

Fit coefficient = 1.000

**ALWAYS – even if wrong**



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## Fit Coefficient

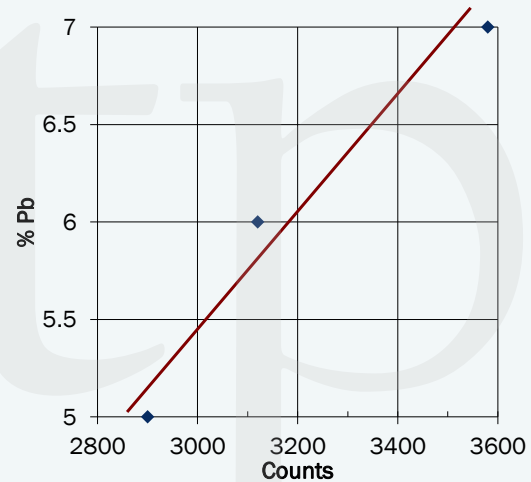
### 3 point calibration

% AC	Counts	Difference
5.0	2900	-0.017
6.0	3120	0.017
7.0	3580	-0.016

Fit Coefficient = 0.998

Straight line fit

**ARDOT 449A requires 3 points**



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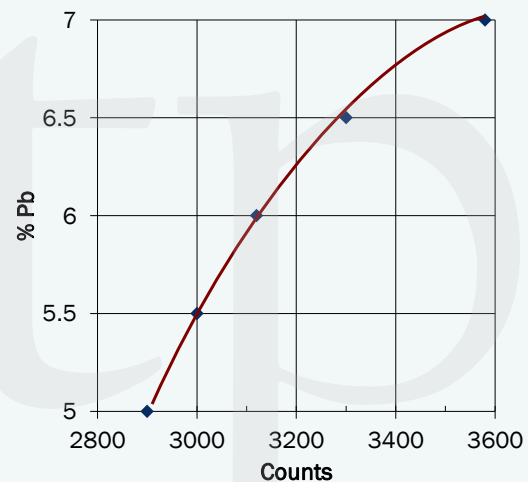
## Fit Coefficient

### 3+ point calibration

% AC	Counts	Difference
5.0	2900	-0.002
5.5	3000	0.001
6.0	3120	-0.001
6.5	3300	0.001
7.0	3580	-0.002

Fit Coefficient ~ 0.999 or greater

Curved fit



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## Use Correct Calibration

Activate appropriate calibration during production for field testing

If > 120 days interruption of mix production has occurred, verify the mix calibration before use

- Prepare sample at design binder content
- Record date, mix design number, and test results



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## Determining Asphalt Binder Content by Ignition Method

AASHTO T 308

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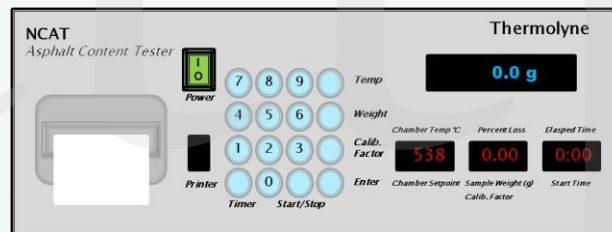
209

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# Ignition Oven Preparation

## Mix Design

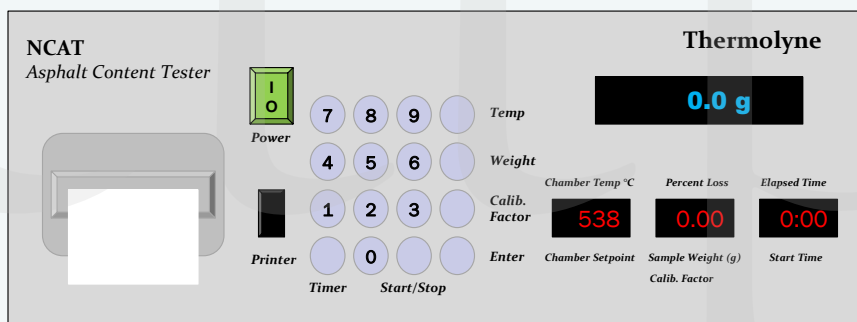
- Preheat ignition oven to calibration temperature
  - 538 °C or 482 °C
- Input appropriate binder content correction (calibration) factor



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# Ignition Oven Control Panel – Entering Data



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## Ignition Oven – Sample Preparation

Obtain a representative asphalt sample according to AASHTO T 97

- Reduce using AASHTO R 47 to appropriate size

Use AASHTO T 329 to dry sample to constant mass

- Mixing temperature or  $325 \pm 25$  °F

**OR**

Determine the moisture content using AASHTO T 329 and subtract from Pb


NMAS	Minimum Mass (g)*
# 4	1200 g
3/8"	1200 g
1/2"	1500 g
3/4"	2000 g
1"	3000 g
1 1/2"	4000 g

*\*max = min + 500g*

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## Ignition Oven Procedure

-  Record the mass of the empty basket assembly

Place 1/2 of the sample into bottom basket

- Flatten and move sample away from basket edges

Repeat for other 1/2 of sample in top basket


Complete basket assembly



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## Ignition Oven Procedure

 Record mass of total basket assembly

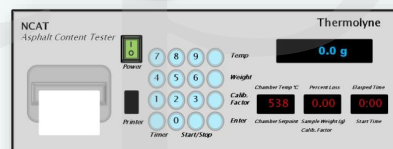
- Sample + basket assembly

Calculate initial mass of asphalt sample

- Net weight of sample
- Input using oven panel

Zero ignition oven scale

- Press "0"



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## Ignition Oven Procedure

Load basket assembly into oven

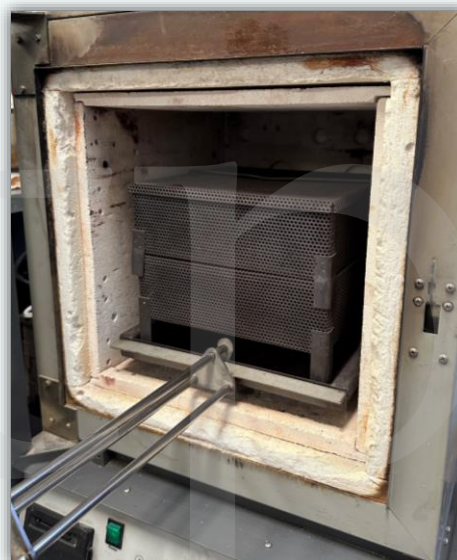
- Maintain clearance on all sides

Close and lock door

Verify total mass

- Within  $\pm 5$  g of recorded total assembly mass

Press start



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## Ignition Oven Procedure

### After burn

- Record binder content from the printed ticket (0.01 %)
- Subtract moisture content
- Report % binder to nearest 0.1 %

### Cool sample

- Save for sieve analysis if needed

Elapsed Time :	57:21
Sample Weight :	1838g
Weight Loss :	84.4g
Percent Loss :	4.59 %
Temp Comp :	0.16 %
Calib. Factor :	0.37 %
<b>Calib. Asphalt Cnt</b>	<b>4.06 %</b>
Filter Set Pt :	850 °C
Chamber Set Pt :	538 °C

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## Determining Correction Factors for the Ignition Oven

AASHTO T 308 – Annex A

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## Ignition Oven - Preparation

Obtain representative samples of binder and aggregate

- Oven dry aggregates

Batch according to job mix formula and  $Pb_{\text{optimum}}$

Batch the asphalt mixture to meet the minimum mass requirements

Do not exceed minimum mass by more than 500g

NMAS	Minimum Mass (g)
# 4	1200 g
3/8"	1200 g
1/2"	1500 g
3/4"	2000 g
1"	3000 g
1 1/2"	4000 g

*\*max = min + 500g*

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## Ignition Oven – Calibrations

Binder Correction Factor

- 2 samples
- Mix at design **optimum** binder content



Aggregate Correction Factor

- 1 sample
- Dry (no binder added)



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## Ignition Oven – Binder Correction Factor

Sample 1



Sample 2



Set calibration factor to 0.00 in ignition oven  
Burn asphalt samples at 538 °C  
Cool aggregate and save for further testing

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## Ignition Oven – Binder Correction Factor

Compare the measured binder contents from the printed tickets

- “Calibrated Asphalt Cntnt”

Elapsed Time:	37:12
Sample Weight:	1687g
Weight Loss:	78.4g
Percent Loss:	4.65%
Temp Comp:	0.14%
Calib. Factor:	0.00%
Calibrated Asphalt Cntnt	
	4.51%

Elapsed Time:	39:25
Sample Weight:	1682g
Weight Loss:	77.0g
Percent Loss:	4.58%
Temp Comp:	0.15%
Calib. Factor:	0.00%
Calibrated Asphalt Cntnt	
	4.43%

Are results within  $\pm 0.15\%$ ?

$$4.51 - 4.43 = 0.08$$



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## Ignition Oven – Binder Correction Factor

If the difference is within 0.15 %:

Average the two results

- Burn 1 4.51 %
- Burn 2 4.43 %

$$\text{Average} = \frac{(4.51 + 4.43)}{2} = 4.47$$

Subtract the actual binder content of the samples

- Samples mixed at 4.1 % ( $P_{b_{\text{optimum}}}$  from mix design)

$$CF_{\text{binder}} = 4.47 - 4.10 = 0.37 \quad \mathbf{0.37 \%}$$

*Report the binder correction factor to the nearest 0.01 %*

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## Ignition Oven – Binder Correction Factor

If the difference exceeds 0.15 %:

- Difference =  $4.49 - 4.31 = 0.18$  ✗

Elapsed Time:	41:57
Sample Weight:	1687g
Weight Loss:	78.1g
Percent Loss:	4.63%
Temp Comp:	0.14%
Calib. Factor:	0.00%
Calibrated Asphalt Cnt	<u>4.49%</u>

Elapsed Time:	40:38
Sample Weight:	1687g
Weight Loss:	75.2g
Percent Loss:	4.45%
Temp Comp:	0.14%
Calib. Factor:	0.00%
Calibrated Asphalt Cnt	<u>4.31%</u>

Elapsed Time:	42:25
Sample Weight:	1686g
Weight Loss:	77.6g
Percent Loss:	4.60%
Temp Comp:	0.15%
Calib. Factor:	0.00%
Calibrated Asphalt Cnt	<u>4.45%</u>

Elapsed Time:	43:12
Sample Weight:	1689g
Weight Loss:	78.7g
Percent Loss:	4.66%
Temp Comp:	0.14%
Calib. Factor:	0.00%
Calibrated Asphalt Cnt	<u>4.52%</u>

Calculate the correction factor

- Samples mixed at 4.1 % ( $P_{b_{\text{optimum}}}$ )

$$CF_{\text{binder}} = \frac{(4.49 + 4.45)}{2} = 4.47 - 4.10 = 0.37 \quad \mathbf{0.37 \%}$$

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## Ignition Oven – Binder Correction Factor

If correction factor  $\leq 1.0\%$  at  $538\text{ }^{\circ}\text{C}$

- Report  $\text{CF}_{\text{binder}}$

If correction factor  $> 1.0\%$  at  $538\text{ }^{\circ}\text{C}$

- Start over but burn samples at  $482\text{ }^{\circ}\text{C}$
- Report  $\text{CF}_{\text{binder}}$  even if  $> 1.0\%$  if established at  $482\text{ }^{\circ}\text{C}$

If there is no improvement in  $\text{CF}_{\text{binder}}$  at  $482\text{ }^{\circ}\text{C}$ , use either CF / temperature

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## Binder Calibration – Problem 1

Determine  $\text{CF}_{\text{binder}}$

Design  $P_b = 5.3\%$

Sample 1       $5.37\%$  @  $538\text{ }^{\circ}\text{C}$

Sample 2       $5.40\%$  @  $538\text{ }^{\circ}\text{C}$

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## Binder Calibration – Problem 2

Determine  $CF_{\text{binder}}$

Design  $P_b = 5.5 \%$

Sample 1	5.78 % @ 538 °C
Sample 2	5.57 % @ 538 °C
Sample 3	5.66 % @ 538 °C
Sample 4	5.80 % @ 538 °C

Diff. = 0.21 

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## Binder Calibration – Problem 3

Determine  $CF_{\text{binder}}$

Design  $P_b = 6.4 \%$

Sample 1	7.92 % @ 538 °C
Sample 2	7.96 % @ 538 °C

Diff. = 0.04 

Average = 7.94

$$CF_{Fbinder} = 7.94 - 6.40 = 1.54$$

$C_F > 1.0 \%$

Sample 3	7.49 % @ 482 °C
Sample 4	7.44 % @ 482 °C

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## Ignition Oven – Aggregate Correction Factors

Use 3 aggregate samples

- (1) Dry aggregate sample
- (2) Burned samples



Record dry weights

Wash aggregate samples over #200 sieve

- Wetting agent required
  - Use enough soap to produce a small amount of suds



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## Ignition Oven – Aggregate Correction Factors

Perform sieve analysis for each sample

- Dry samples to constant mass
- Cool
- Record dry weight after wash
- Sieve samples
- Report % passing to nearest 0.1 % for all sieves



Record dry weight after wash

Sieve samples

Report % passing to nearest 0.1 % for all sieves



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## Ignition Oven – Aggregate Correction Factors

Average % passing for the 2 burned samples

Sieve	True		Measured	
	Blank	Burn # 1	Burn # 2	Average Burn
1/2"	94.3	97.2	97.0	97.1
3/8"	85.9	87.6	87.8	87.7
# 4	54.3	55.8	56.0	55.9
# 8	36.7	37.9	37.5	37.7
# 16	26.1	29.5	29.7	29.6
# 30	17.7	18.8	19.0	18.9
# 50	11.9	12.6	12.8	12.7
# 100	8.5	9.0	8.6	8.8
# 200	4.6	4.9	5.1	5.0

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## Ignition Oven – Aggregate Correction Factors

Subtract the average burn from the blank sample

Sieve	True		Measured		True – Measured
	Blank	Burn # 1	Burn # 2	Average Burn	
1/2"	94.3	97.2	97.0	97.1	-2.8
3/8"	85.9	87.6	87.8	87.7	-1.8
# 4	54.3	55.8	56.0	55.9	-1.6
# 8	36.7	37.9	37.5	37.7	-1.0
# 16	26.1	29.5	29.7	29.6	-3.5
# 30	17.7	18.8	19.0	18.9	-1.2
# 50	11.9	12.6	12.8	12.7	-0.8
# 100	8.5	9.0	8.6	8.8	-0.3
# 200	4.6	4.9	5.1	5.0	-0.4

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## Ignition Oven – Aggregate Correction Factors

Compare each ACF to the allowable difference

Sieve	Blank	Burn # 1	Burn # 2	Average Burn	ACF	Allowable Diff.
1/2"	94.3	97.2	97.0	97.1	-2.8	± 5 %
3/8"	85.9	87.6	87.8	87.7	-1.8	± 5 %
# 4	54.3	55.8	56.0	55.9	-1.6	± 5 %
# 8	36.7	37.9	37.5	37.7	-1.0	± 5 %
# 16	26.1	29.5	29.7	29.6	-3.5	± 3 %
# 30	17.7	18.8	19.0	18.9	-1.2	± 3 %
# 50	11.9	12.6	12.8	12.7	-0.8	± 3 %
# 100	8.5	9.0	8.6	8.8	-0.3	± 3 %
# 200	4.6	4.9	5.1	5.0	-0.4	± 0.5 %

*If any ACF > allowable,  
and if larger than #200,  
then use ALL ACF values*

*If only #200 > allowable,  
use only #200 value*

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## Ignition Oven – Aggregate Correction Factors

Add the appropriate ACFs to the field test results and round

Sieve	Blank	Burn # 1	Burn # 2	Average Burn	ACF	Allowable Diff.	Field Test	Calc. % Pass	Report % Pass
1/2"	94.3	97.2	97.0	97.1	-2.8	± 5 %	97.2	94.4	94
3/8"	85.9	87.6	87.8	87.7	-1.8	± 5 %	88.3	86.5	87
# 4	54.3	55.8	56.0	55.9	-1.6	± 5 %	55.9	54.3	54
# 8	36.7	37.9	37.5	37.7	-1.0	± 5 %	37.8	36.8	37
# 16	26.1	29.5	29.7	29.6	-3.5	± 3 %	29.5	26.0	26
# 30	17.7	18.8	19.0	18.9	-1.2	± 3 %	18.8	17.6	18
# 50	11.9	12.6	12.8	12.7	-0.8	± 3 %	12.6	11.8	12
# 100	8.5	9.0	8.6	8.8	-0.3	± 3 %	9.0	8.7	9
# 200	4.6	4.9	5.1	5.0	-0.4	± 0.5 %	5.2	4.8	4.8

Whole #s

0.1%

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## Problem 1

Determine ACF values and which ones to apply

Sieve	Blank	Burn # 1	Burn # 2	Average Burn	ACF	Allowable Diff.
1/2"	100.0	100.0	100.0	100.0		± 5 %
3/8"	95.2	97.2	97.5	97.4		± 5 %
# 4	73.4	77.6	78.0	77.8		± 5 %
# 8	43.6	46.9	46.7	46.8		± 5 %
# 16	30.7	34.1	34.7	34.4		± 3 %
# 30	20.3	18.8	22.5	23.1		± 3 %
# 50	16.5	18.9	19.4	19.2		± 3 %
# 100	12.0	14.0	13.8	13.9		± 3 %
# 200	6.3	7.3	7.0	7.2		± 0.5 %

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## Problem 2

Determine ACF values and which ones to apply

Sieve	Blank	Burn # 1	Burn # 2	Average Burn	ACF	Allowable Diff.
1/2"	100.0	100.0	100.0	100.0		± 5 %
3/8"	93.4	97.2	95.2	96.2		± 5 %
# 4	68.9	70.2	69.7	70.0		± 5 %
# 8	45.6	46.9	46.2	46.6		± 5 %
# 16	28.4	30.6	30.1	30.4		± 3 %
# 30	19.5	20.2	21.1	20.7		± 3 %
# 50	14.3	17.2	16.3	16.8		± 3 %
# 100	9.8	10.7	11.0	10.9		± 3 %
# 200	4.5	5.1	4.8	5.0		± 0.5 %

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## Problem 3

Determine ACF values and apply as appropriate

Sieve	Blank	Burn # 1	Burn # 2	Average Burn	ACF	Allowable Diff.	Field Test	Calc. % Pass	Report % Pass
1/2"	100.0	100.0	100.0	100.0		± 5 %	100.0		
3/8"	97.4	97.2	98.9	98.1		± 5 %	96.5		
# 4	61.3	65.4	63.6	64.5		± 5 %	65.4		
# 8	38.5	40.1	41.0	40.6		± 5 %	38.1		
# 16	22.6	24.1	23.8	24.0		± 3 %	24.0		
# 30	19.4	19.7	19.9	19.8		± 3 %	20.5		
# 50	16.7	17.8	17.0	17.4		± 3 %	17.7		
# 100	12.3	14.1	13.8	14.0		± 3 %	13.9		
# 200	7.2	8.2	7.6	7.9		± 0.5 %	7.9		

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## Ignition Oven Correction Factors

Correction Factors are mix-specific

- On mix design

Must be determined prior to acceptance testing

Repeat for changes to JMF

- >5% change in gradation

Aggregate correction factor is most critical for aggregates with a history of breakdown

**Design Summary**

Mix Design #: HMA684-25

Total Asphalt Content %: 4.1

New Asphalt Content %: 4.1

Max. Theor. SG (Gmm): 2.437

Asphalt Binder: PG 70-22

Asphalt Binder Source: Hog Oil Company

Mixing Temp (F): 330

Compaction Temp (F): 305

Antistrip Source: Hog Oil 975

Antistrip %: 0.25

% Retained Stability: 94.1

APA Results: 1.951

Spec Max = 5 000 mm

**Volumetric Mix Design**

Mix Type: 25.0 MM ACHM Surface

Air Voids (Va): 4.0

VMA: 13.0

VMA Corr. Factor: 0.3

Gsb: 2.578

Gse: 2.588

Gb: 1.031

Ni: 7

Ndes: 75

Nmax: 115

**Ignition Oven Correction Factors**

Mix Design: TBD

RAP: N/A

RAS: N/A

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# Gradation Test

Determined from the aggregate blend after binder has been removed

- AASHTO T 30
  - Ignition Oven
- ARDOT 460
  - Solvent Wash



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# Mechanical Analysis of Extracted Aggregate

AASHTO T 30


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## Gradation Procedure (AASHTO T 30)

 After cooling, record total weight of basket assembly

 Calculate and record dry weight of aggregate


- Subtract weight of empty basket assembly

2024

Wash aggregate over #200 sieve

- Use a wetting agent
- #8 or #16 cover sieve

Dry to constant mass

 Record mass after wash


- 0.1 %

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## Gradation Procedure (AASHTO T 30)


Sieve sample

- 
- Record weights retained
  - Verify sum of individual weights are within 0.2 % of the mass after wash

Calculate % passing to the nearest 0.1 %

Apply appropriate aggregate correction factors

Report

- 
- All sieves except #200 to the nearest whole number
  - Report #200 sieve to the nearest 0.1 %

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# Solvent Wash and Sieve Analysis of Asphalt Concrete

ARDOT 460

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## Solvent Wash Procedure

Determine binder content

- ARDOT 449

Reduce to an appropriate size

 Record sample weight

Cool to approximately 200 °F

NMAS (inches)	NMAS (mm)	Minimum Wt. of Test Specimen
½"	12.5	1500 g
¾"	19	2000 g
1"	25	3000 g
1 ½"	37.5	4000 g
2 ½"	62.5	4000 g

ARDOT 460

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## Solvent Wash Procedure

Cover sample with solvent

- Stir and soak



Pour solvent over nested #8 and #200 sieves

Repeat washing until solvent maintains its original color

Wash over # 200 sieve using water

- Liquid dish detergent may help remove oily residue



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## Solvent Wash Procedure


Return aggregate retained on sieves to container

Dry to constant mass

- Cool

 Record dry weight after wash


Sieve sample

 • Record weights

Calculate % passing

$$\text{Agg Wt} = \text{Mix Wt} \times \frac{P_s}{100}$$

Report

- All sieves except #200 to the nearest whole number
-  • Report #200 sieve to the nearest 0.1 %

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## Solvent Wash Calculation

Given an asphalt sample weighing 1853.4 g and a  $P_b$  of 6.2 %, find the weight of aggregate to be used in calculating a sieve analysis from a solvent wash

$$\text{Agg Wt} = \text{Mix Wt} \times \frac{P_s}{100}$$

$$P_s = 100 - 6.2 = 93.8$$

$$\text{Agg Wt} = 1853.4 \times \left( \frac{93.8}{100} \right) = (1853.4)(0.938) = 1738.489...$$

$$1738.5 \text{ g}$$

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## Solvent Wash Calculation

Given an asphalt sample weighing 3384.2 g and a  $P_b$  of 5.3 %, find the weight of aggregate to be used in calculating a sieve analysis from a solvent wash

$$\text{Agg Wt} = \text{Mix Wt} \times \frac{P_s}{100}$$

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# Batching & Mixing Asphalt Mixtures

ARDOT 449A

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## Batching

Forms precise gradation in the lab according to the mix design

**Careful batching produces repeatable results!**

Mix designs

Calibrations

Requirements

- % Binder
- Cold Feed %

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## Batching

Collect binder samples

- Manufacturer
- PG Grade

Collect representative stockpile samples

- Oven dry aggregates
- Fractionate if needed

Determine the size of sample to be batched

- See specification

Determine the number of “points” to be batched

- See specification

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## Batch Weights (Aggregate)

Determine the aggregate batch weights if the required total aggregate weight is 10,000 g

<u>Aggregate</u>	<u>%</u>		<u>Weight</u>
B Rock	28	$(0.28)(10,000)$	= 2,800
5/8" Chips	25	$(0.25)(10,000)$	= 2,500
1/4" Scrn.	29	$(0.29)(10,000)$	= 2,900
Man. Sand	15	$(0.15)(10,000)$	= 1,500
Sand	3	$(0.03)(10,000)$	= 300
<b>Total</b>	<b>= 100</b>	<b>Total</b>	<b>= 10,000</b>

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## Batch Weights (Aggregate)

Determine the aggregate batch weights if the required total aggregate weight is 8,000 g

<u>Aggregate</u>	<u>%</u>
3/4" Chip	30
1/2" Screen	28
1/4" Screen	25
Ind. Sand	17

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## Batch Weights (Mix)

Determine the batch weights if the desired mix weight is 1,700 g and the binder content is 6.0 %

<u>Material</u>	<u>%</u>		<u>Weight</u>
Binder	6.0	$(0.06)(1,700)$	= 102.0
$P_S = 100\% - 6.0\% = 94.0\%$			
Aggregate		$(0.94)(1,700)$	= 1,598.0
3/4" Chip	36	$(0.36)(1,598)$	= 575.3
1/2" Chip	40	$(0.40)(1,598)$	= 639.2
Ind. Sand	24	$(0.24)(1,598)$	= 383.5
<b>Total</b>	<b>= 100</b>	<b>Total Agg</b>	<b>= 1,598.0</b>

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## Batch Weights (Mix)

Determine the batch weights if the desired mix weight is 3,300 g and the binder content is 5.2 %

Material	%
Binder	5.2
<b>Aggregate</b>	
3/4" Chip	35
1/2" Chip	32
Ind. Sand	33
<b>Total</b>	<b>= 100</b>

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## Mixing

Preheat oven to mixing temperature

- Mix design

Heat aggregate to mixing temp

- 2 – 4 hours minimum
- May be heated overnight
- RAP/RAS not preheated with aggregate

Heat binder to mixing temperature

- 1 – 2 hours prior to mixing
- Do not heat overnight!

Preheat tools and mixing bucket

- Clean and/or “butter” mixing bucket
- Prevents low binder content on the first mixed batch

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## Mixing

Zero mixing pot on scale

- Scale must be readable to 0.1 g



Add aggregate to mixing bucket

- Mix aggregate
- Form crater for binder



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## Mixing

Get aggregate weight

Calculate either:

- Mix weight **OR** binder weight

$$\text{Mix Wt} = \frac{\text{Agg Wt}}{P_s} \times 100$$

$$\text{Binder Wt} = \text{Mix Wt} - \text{Agg Wt}$$

Add binder to crater



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## Mixing

Determine the mix weight or binder weight for a sample if the Pb = 5.6 % and the measured weight of aggregate in the mixing bucket is 7998.2 g.

$$\text{Mix Wt} = \frac{\text{Agg Wt}}{P_s} \times 100$$

$$P_s = 100 - 5.6 = 94.4$$

$$\text{Mix Weight} = \frac{7998.2}{94.4} \times 100 = 8472.7$$

$$\text{Binder Weight} = 8472.7 - 7998.2 = 474.5$$

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## Mixing

Determine the mix weight or binder weight for a sample if the Pb = 4.4 % and the measured weight of aggregate in the mixing bucket is 4,995.0 g

$$\text{Mix Wt} = \frac{\text{Agg Wt}}{P_s} \times 100$$

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## Mixing

Adjust to obtain the exact weight of binder



Mix thoroughly for at least 2 minutes



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## Mixing

Empty mixing bucket

- Use hot spatula or spoon to scrape out all of the mixture
- Scrape tools

Place all scraped material into the sample container



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## Mixing

Verify mixing bucket is within  $\pm 5$  g of its initial weight

- If not, keep scraping!
- Reheat mixing pot if necessary



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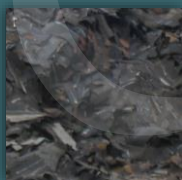
276

## Mixing RAP / RAS



### RAP

- Reclaimed Asphalt Pavement
- Add to aggregate 1 hour before mixing



### RAS

- Recycled Asphalt Shingles
- Add to aggregate at time of mixing

*Treated as aggregate portions*

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## Compaction and Density

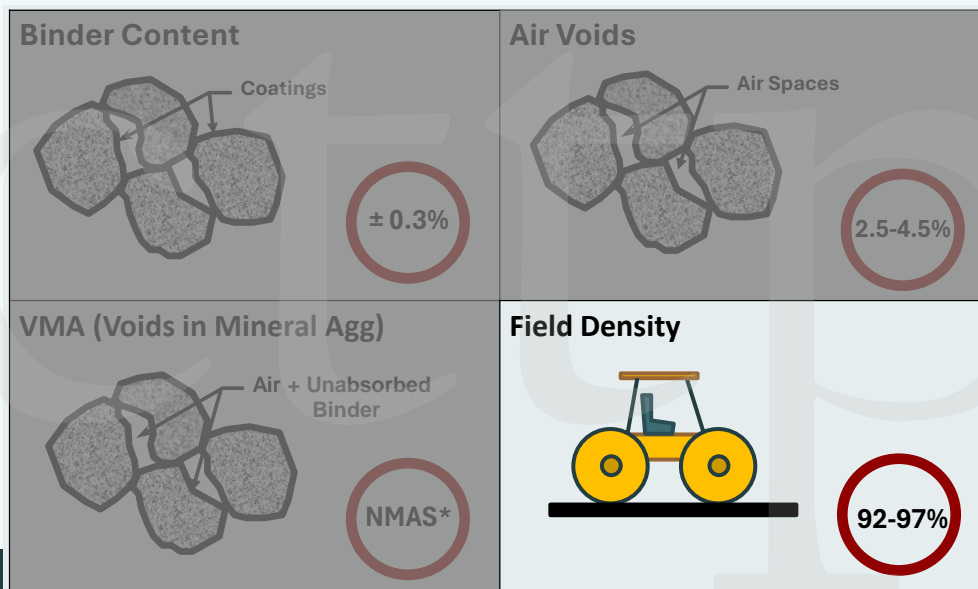
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## Prepare Samples for QC/QA Testing



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# Compaction

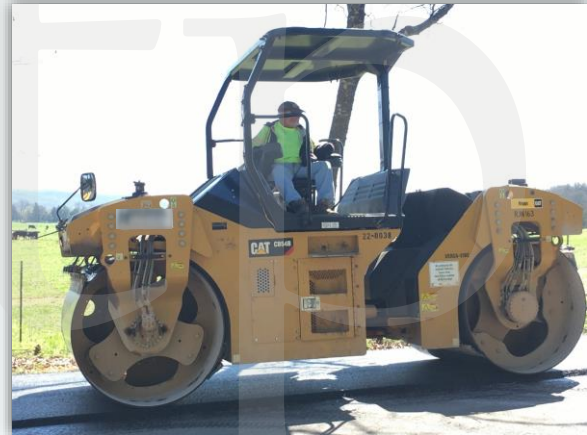
The MOST IMPORTANT factor affecting performance

- Compaction is a process
- Density is a measurement

Intelligent compaction

Best practices

- Stay close to the paver
- Angle drum when changing direction
- Never park roller on mat
- Start/stop slowly, vary location



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# Rollers

Steel wheel

- Breakdown – vibratory mode



- Finish – static mode

Pneumatic

- Intermediate
- Knead particles



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## Rolling Pattern

ARDOT 410.08 – Rolling patterns are established at the beginning of placement for each mix design on a project

### Equipment

- Nuclear density gauge
- Electromagnetic surface contact device
  - ASTM D7113



***If the compaction method or equipment is changed, a new rolling pattern shall be established***

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## Rolling Pattern

Pattern to achieve specified density

- Type or roller
- # vibratory passes
- # static passes

Take a 15 second wet density (WD) reading with gauge after every roller pass until no further increase in density

Take all readings at exact same location



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## Rolling Pattern

Choose only passes that increase density

Roller	Pass	Vibratory Static	WD Reading
Break	1	Vib	140.2
Dual	2	Vib	143.4
	3	Vib	146.5
	4	Static	147.0
	5	Static	145.3
	6	Static	144.7
Inter			
Rub	1	Static	147.8
	2	Static	148.1
	3	Static	147.2
	4	Static	147.2

Rolling Pattern:

- 3 vibratory passes with breakdown roller
- 1 static pass with breakdown roller
- 2 static passes with pneumatic roller

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## Sampling Asphalt Mixtures after Compaction (Obtaining Cores)

AASHTO R 67

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## Coring Equipment

Core drill

Diamond-edged drill bit

Cooling agent

- Water, ice, dry ice, liquid nitrogen

Retrieval device

Separation equipment

- Hammer and chisel
- Wet saw



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## Coring Procedure

Allow mat to cool

Cut core perpendicular to surface

- Use water or air while drilling
  - Reduces heat
- Apply constant, gradual pressure
- Drill to bottom of layer
  - Or slightly below

Remove core

- If damaged, cut another core within 6 inches of original

Label core

Fill hole with asphalt mixture

- Compact mixture
- Level with surface

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## Transporting Cores

Secure cores against jarring, rolling, or impact with any objects

- Newspaper
- Cylinder molds

Protect against extreme temperatures

- Insulated container



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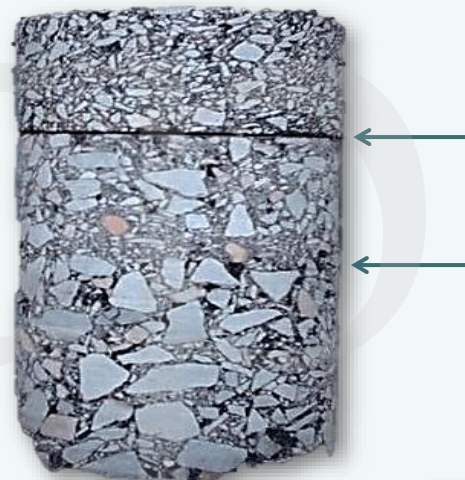
289

## Separating Layers

Separate cores at the point of bonding

- Hammer and chisel
- Wet saw

Remove tack coats and bound gravel or dirt before testing



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## Density Specification (ARDOT)

Cut one core for every lot/sublot test

- Cut full depth cores
- 4" minimum diameter
- Label core

Standard Spec – 410.09

- Leveling and bond breakers
  - Thickness must be 3x NMAS

***Do not sample within 1.5 feet of the edge  
(different for joint densities)***



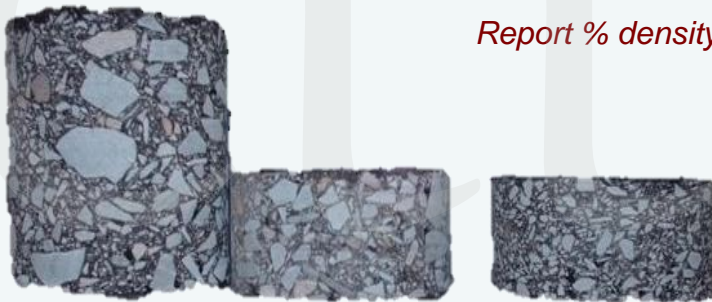
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## Density

$$\% \text{ Density} = \frac{G_{mb}}{G_{mm}} \times 100$$

*Report % density to the nearest 0.1 %*



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## Joint Density

ARDOT Special Provision

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## ARDOT Joint Density (SP)

Must cut 6" cores

Must use notched wedge  
unless milled or cutback

← 2025

Final surface

- Lot = 40,000 linear feet
- Sublot = 10,000 linear feet
- 90% - 96% density
  - Use average Gmm
- If < 88% density, seal with PG 64-22

← 2025

← 2025

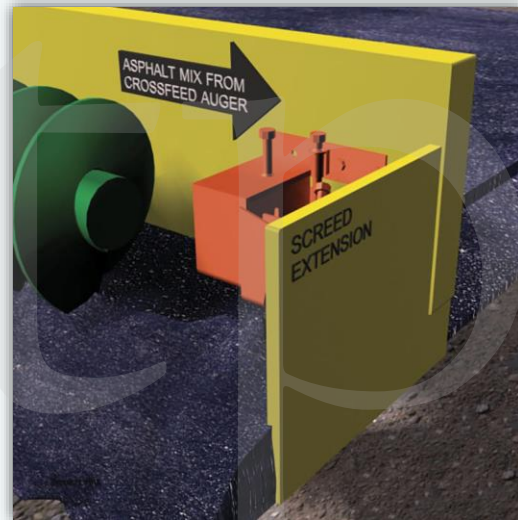


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## Notched Wedge Joint



<https://transtechsys.com>

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## Butt Joint



Cannot use Notched Wedge for milled or cutback joints

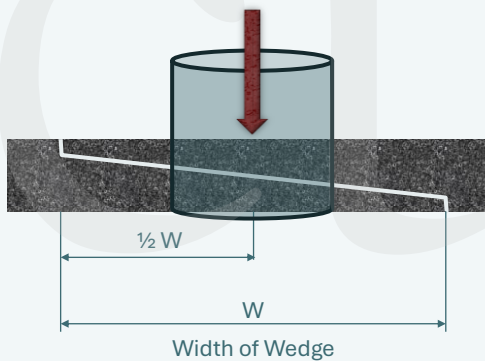
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## Center of the Joint

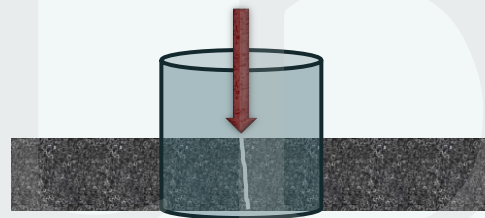
### Notched Wedge Joints

- Centered over wedge width



### Milled or Cutback Joint

- Centered over visible joint line



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## Notched Wedge Joint



Measure before the "hot" lane is placed

Inform the core drill operator

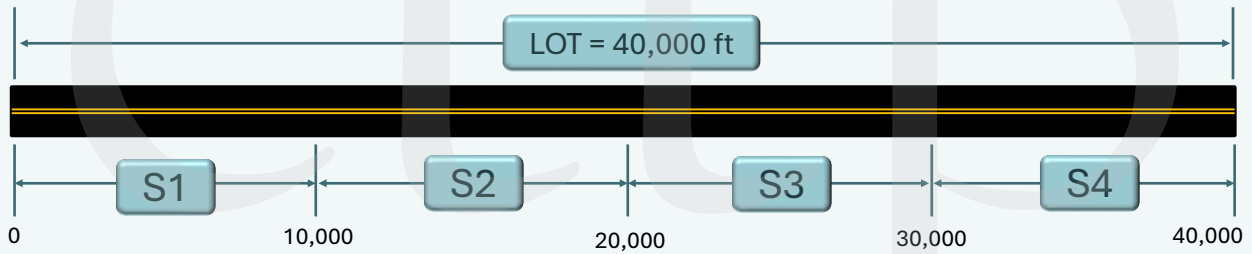
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## Joint Density Location

Only where joints are formed

- Centerline, lane lines
- Not shoulder



**Joint density locations will not match mat density locations!**

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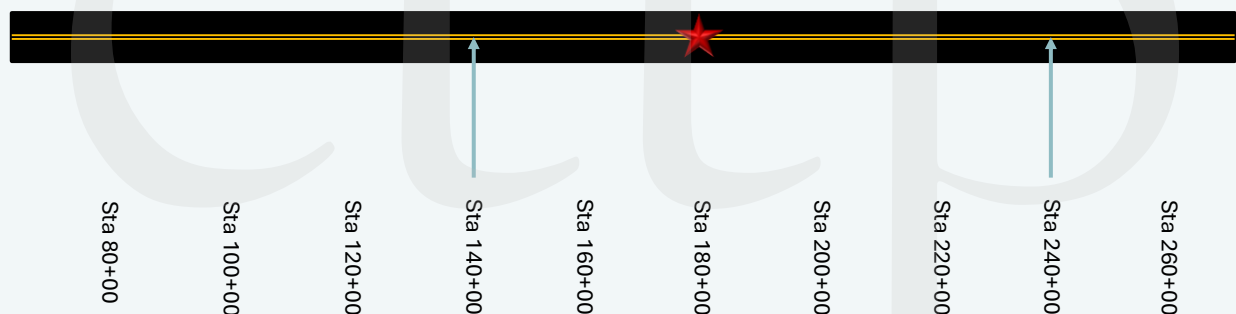
## Joint Density Location

Sample between Sta. 140+00 to 240+00 and RN = 0.38

Determine the station location and Gmm required for testing

$$10,000 \times 0.38 = 3800$$

$$14,000 + 3800 = 17,800 \text{ (Sta 178+00)}$$



300

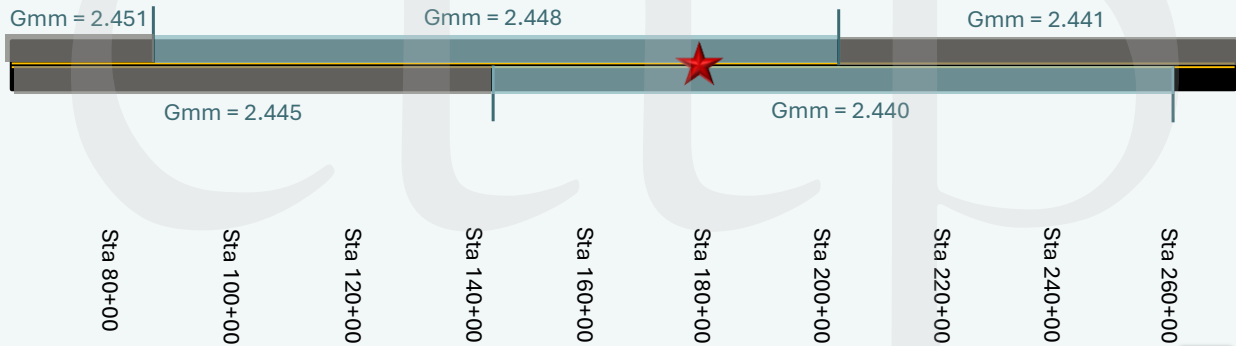
300



## Joint Density Location

$$\text{Gmm}(\text{avg}) = \frac{2.448 + 2.440}{2} = 2.444$$

**Test at Sta. 178+00**  
**Use Gmm value of 2.444**



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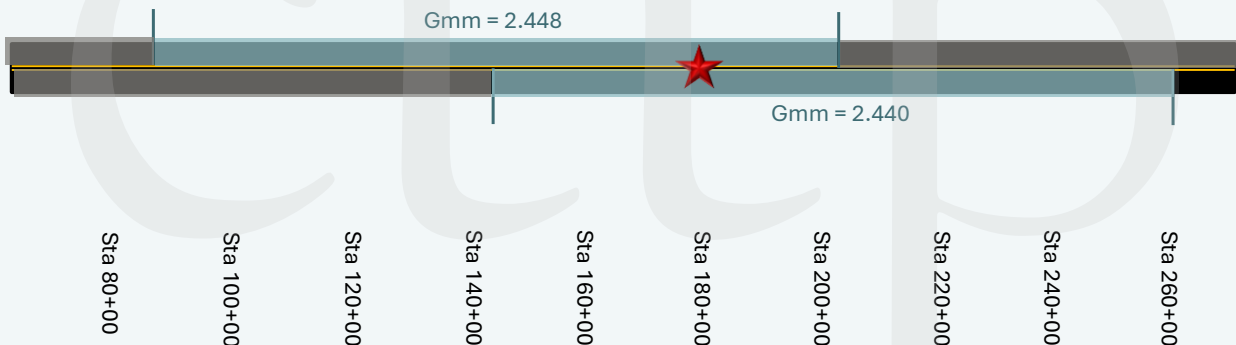
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## Joint Density Calculation

$$\% \text{ Density} = \frac{2.229}{2.444} \times 100 = 91.2029\ldots$$

**Test at Sta. 178+00**  
**Use Gmm value of 2.444**  
**Gmb = 2.229**

**91.2% Density**



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# Inertial Profiling

International Roughness Index (IRI)

- Ride quality

Primary types

- Lightweight
- High-Speed



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# Quality

What defines quality?

What do we measure?

How good is good enough?

How often to test?

Variability in process

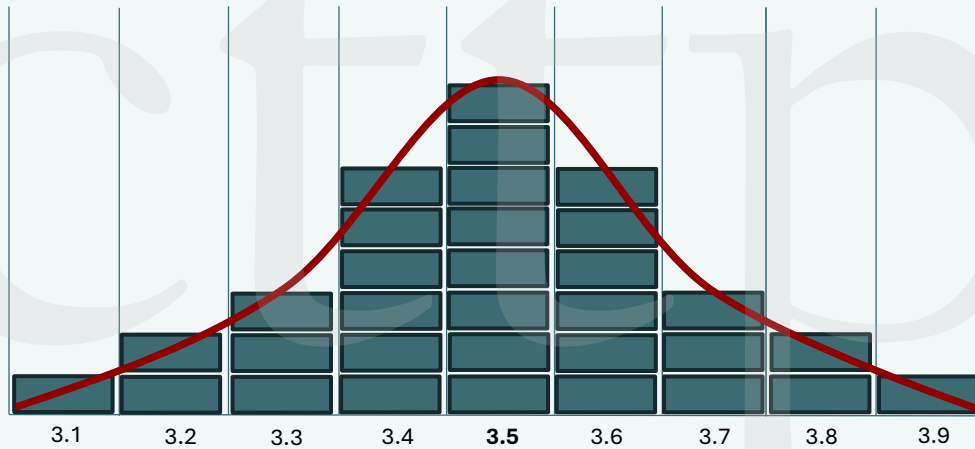
- Materials
- Procedure
- Construction



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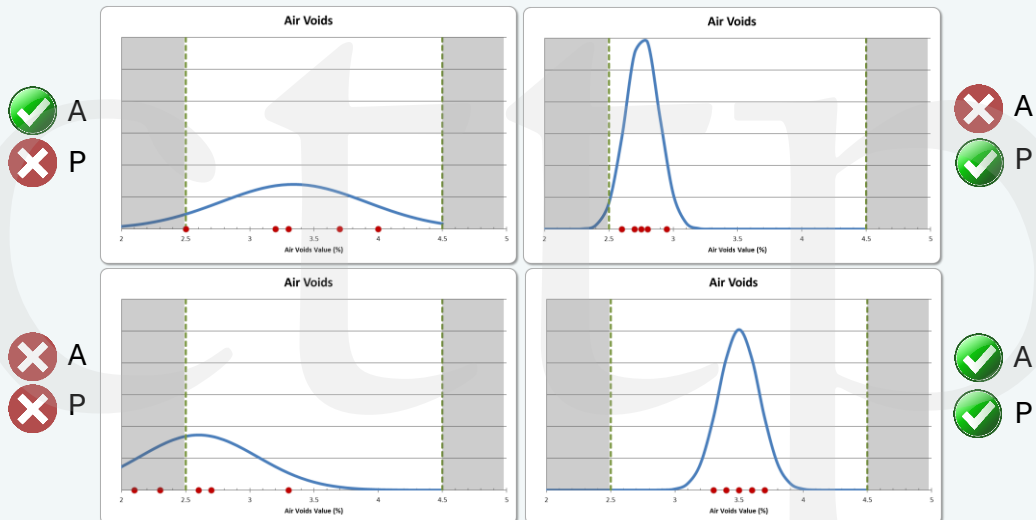
## Frequency Diagram



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## Percent Within Limits

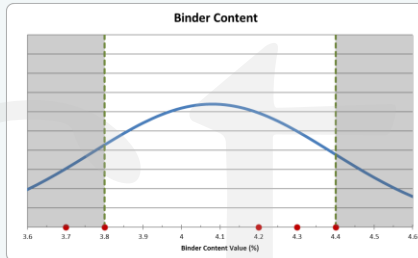


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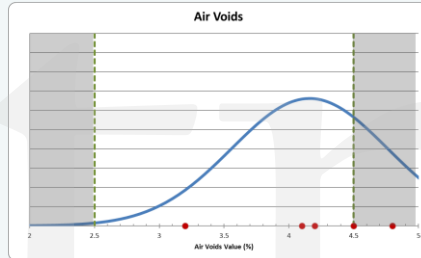
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# Pay Factors

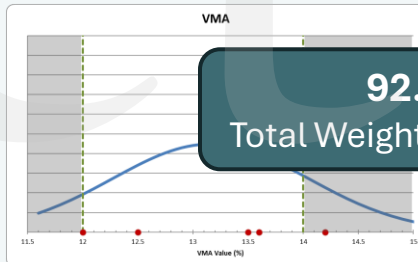
PWL = 65.14%  
PF = 85.57%  
(20%)



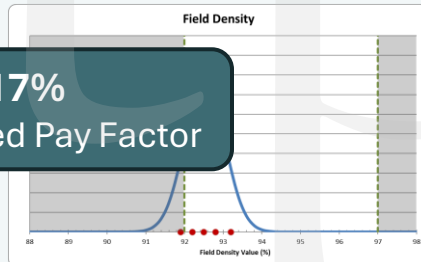
PWL = 69.60%  
PF = 89.80%  
(35%)



PWL = 73.63%  
PF = 91.82%  
(10%)



PWL = 84.52%  
PF = 97.26%  
(35%)



**92.17%**  
**Total Weighted Pay Factor**

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